



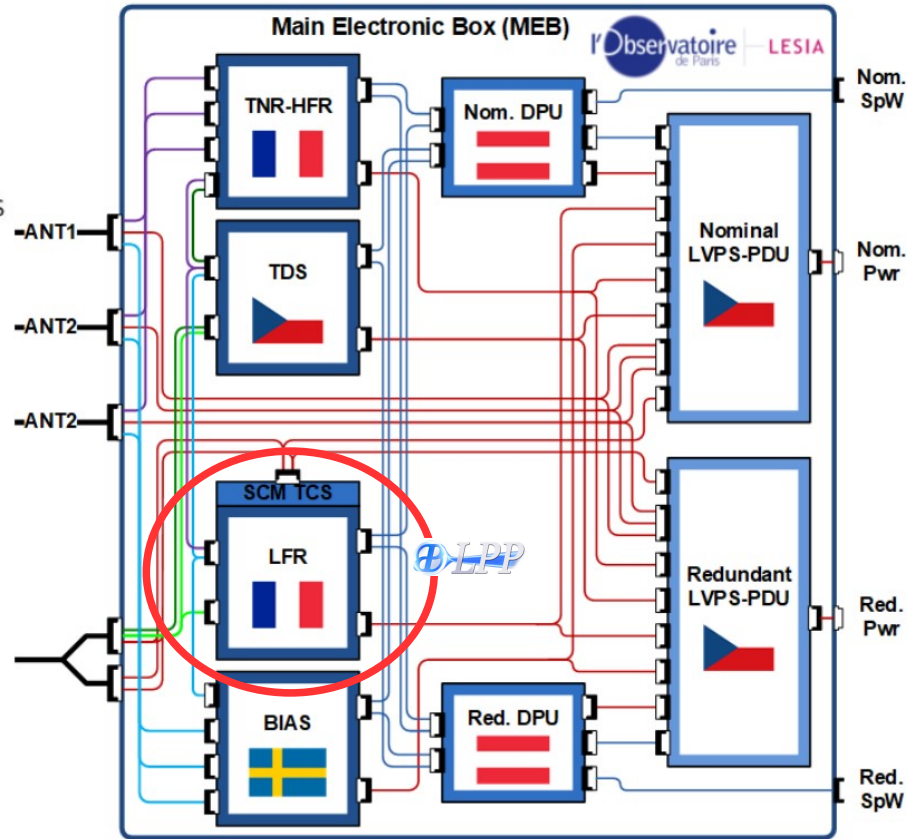
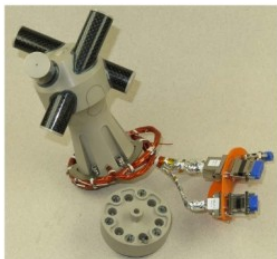
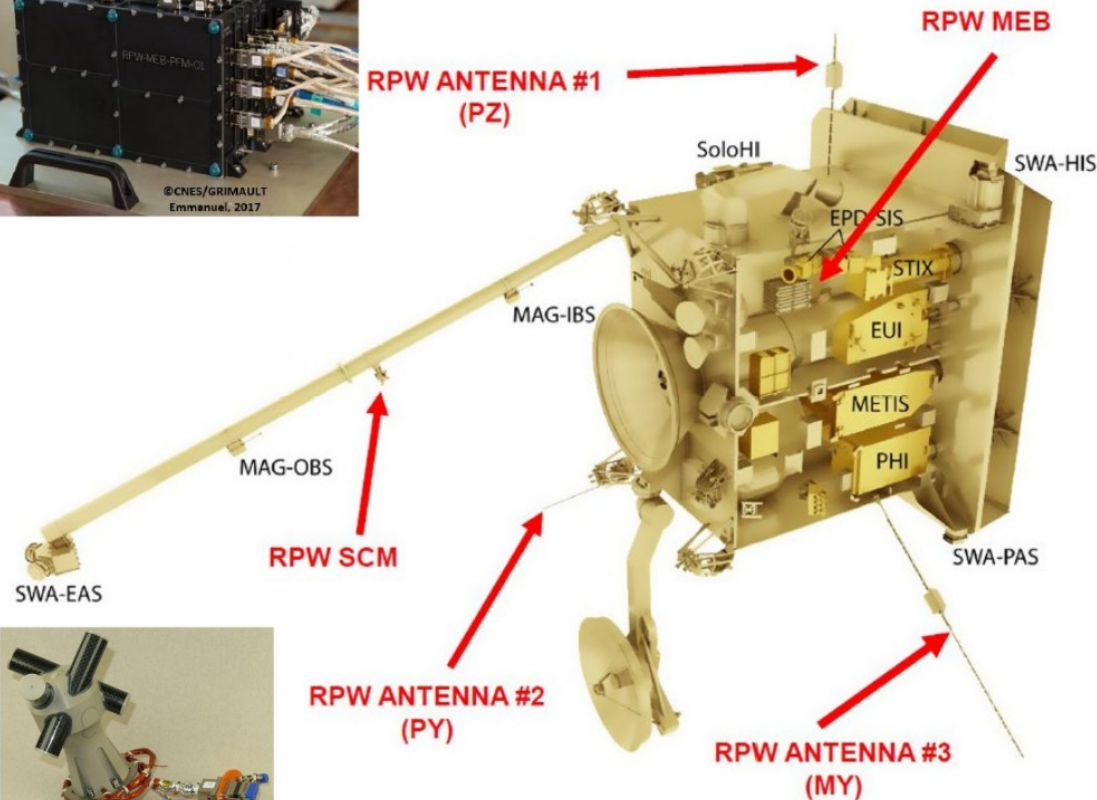
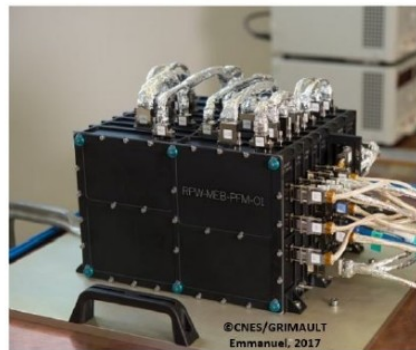
Low Frequency Receiver - LFR

In-flight performance and observations of whistler mode waves

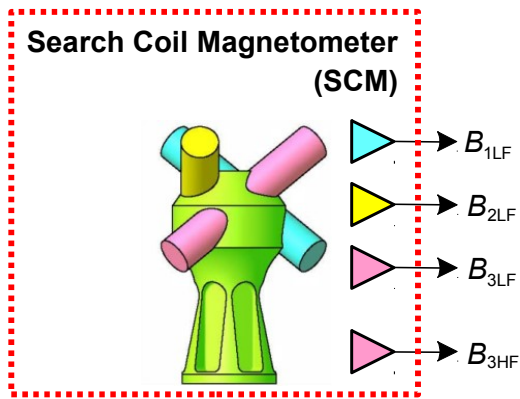
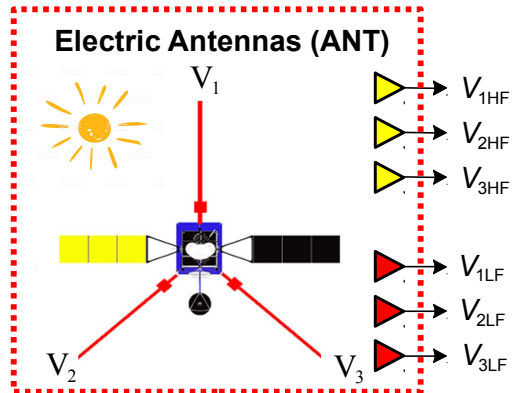
Thomas Chust, the LFR team and the RPW instrument consortium



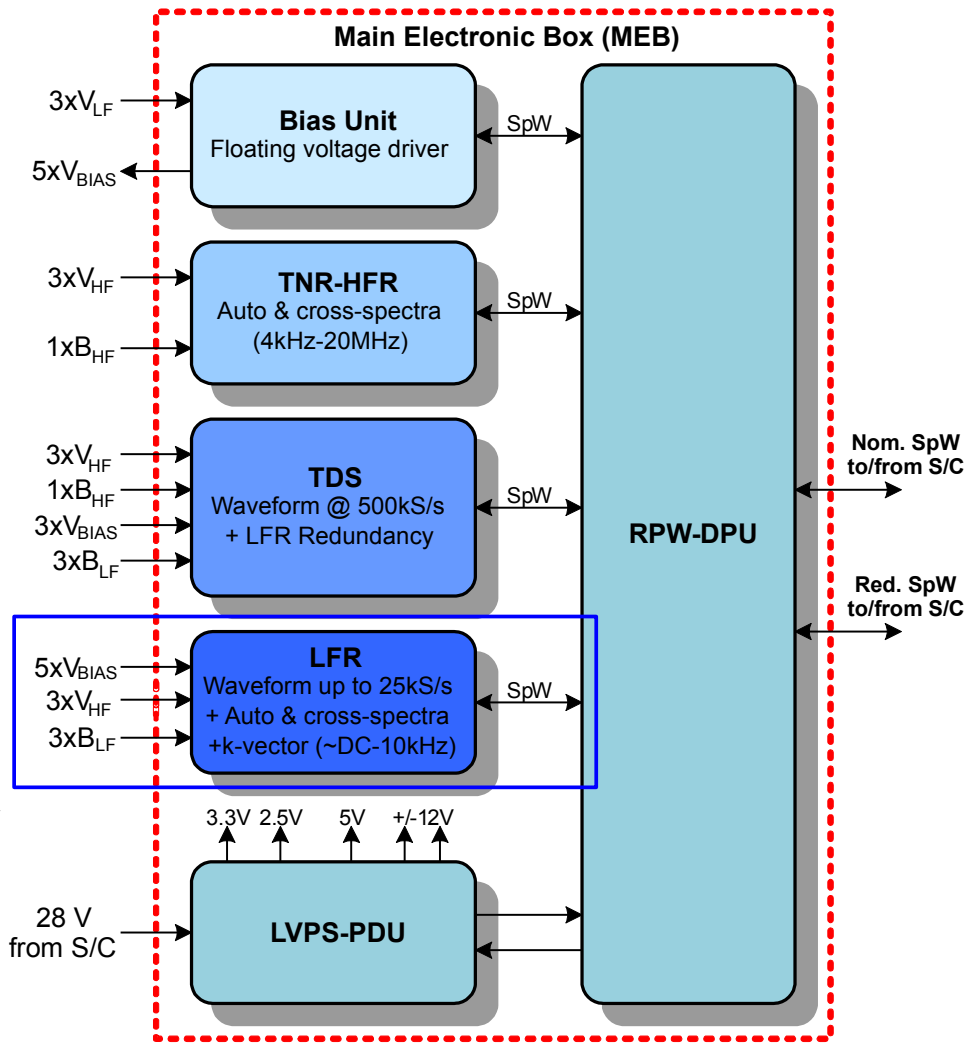
The instrument



RPW Instrument Overview



Low Frequency Receiver



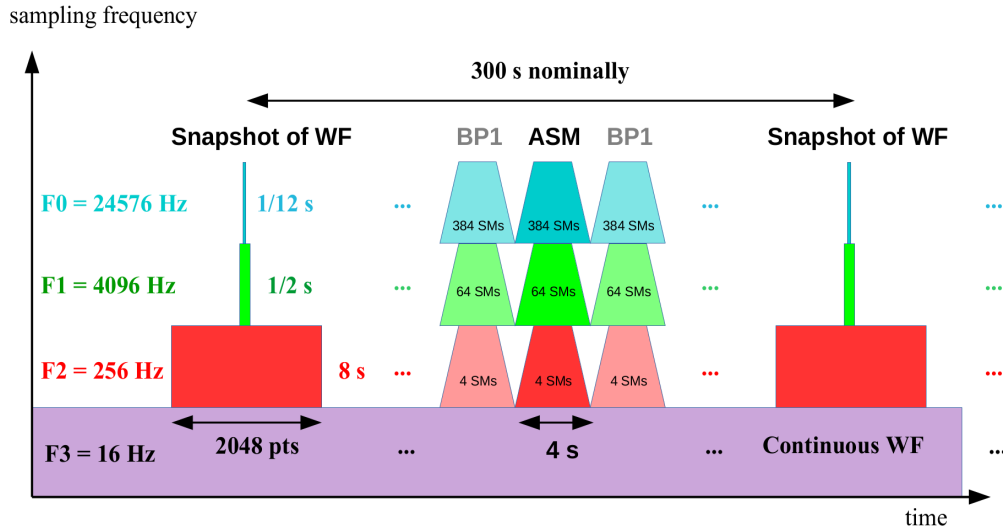
LFR nominal inputs : $3 B + 2 E + 1 V (\leq 10 \text{ kHz})$,

The LFR signal processing, based on a FPGA, provides routinely,

- waveforms (SWF & CWF)
- spectral matrices (ASM & BP2)
- basic wave parameters (BP1)

at different time and frequency resolutions:

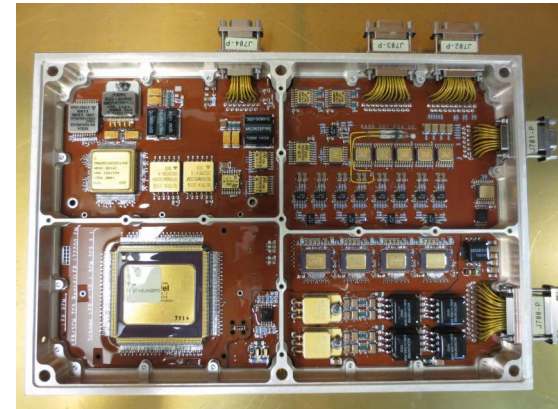
LFR Normal Mode data flow



LFR data are calibrated at LESIA by the **ROC production pipeline**, using the calibration softwares of the teams (SCM, BIAS & LFR):

- SCMCAL (LPCE2, Orléans, France)
- BICAS (IRF, Uppsala, Sweden)
- LFR-CALBUT (LPP, Palaiseau, France)

Despite the fact that calibrations of the E and B data still require some improvement (phase shift issue, effective antenna lengths), the first results obtained so far show a **good overall consistency of the RPW LFR data** (A&A 2021 special issue papers, about 12 papers)




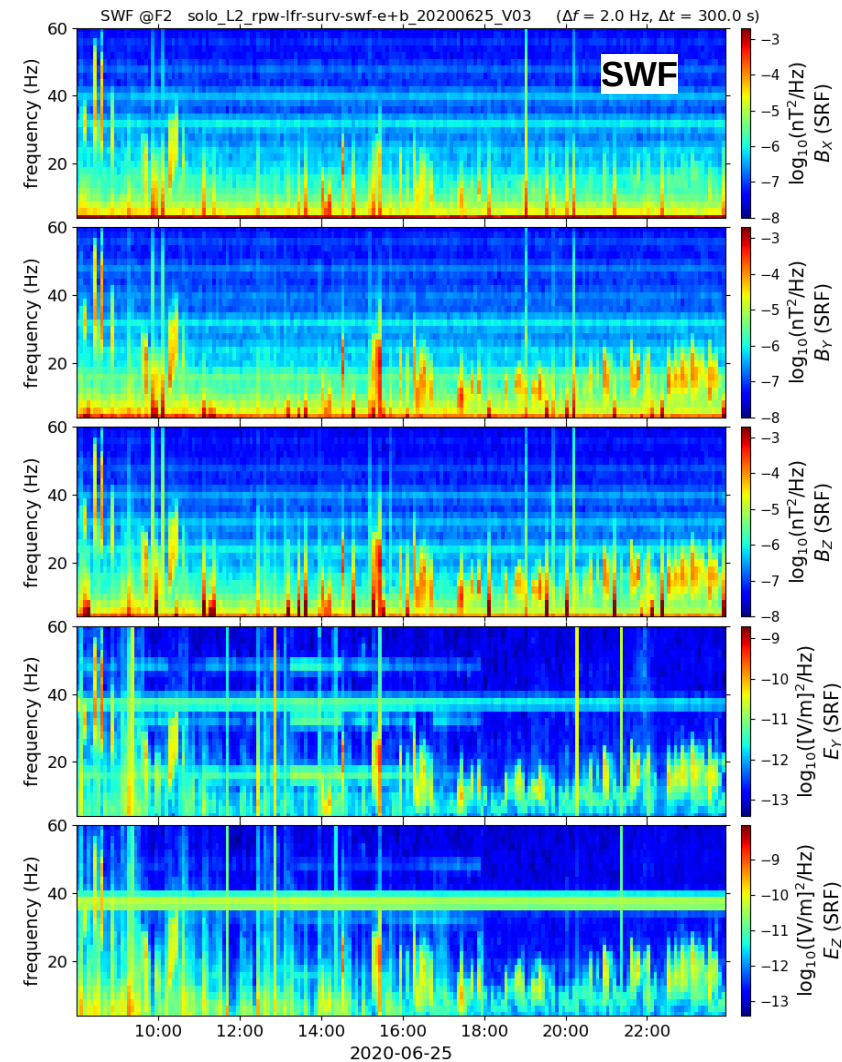
LFR FM board

Solar Orbiter First Results (Cruise Phase)

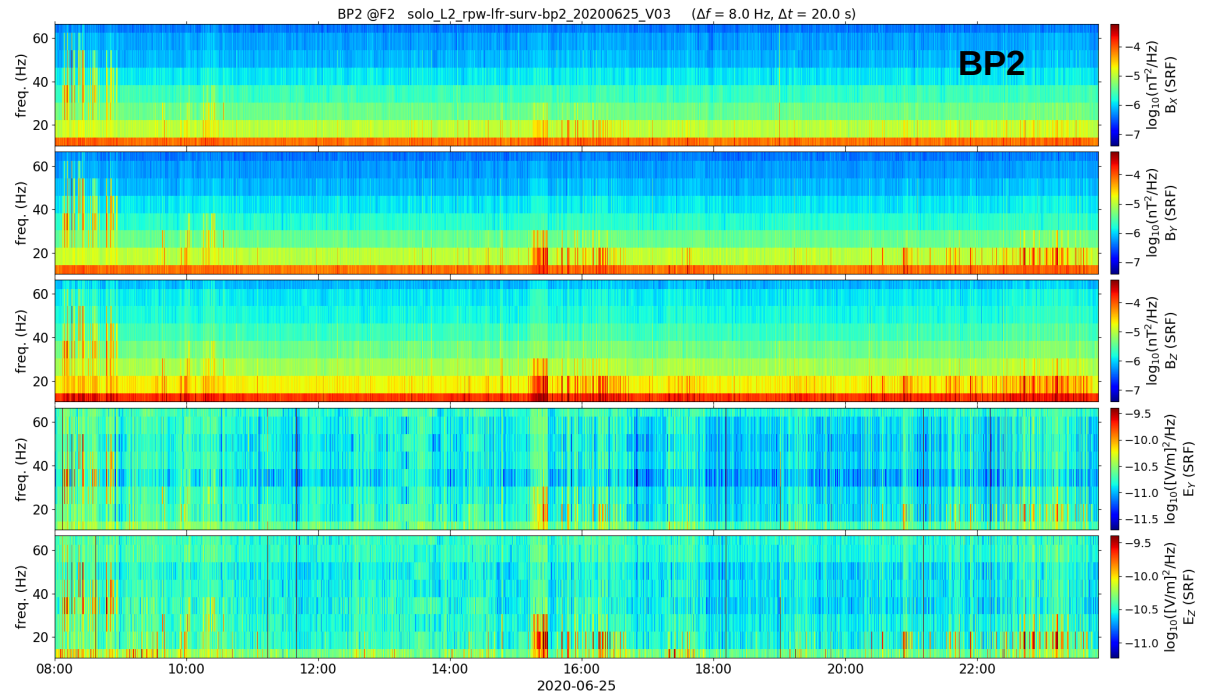
Special issue

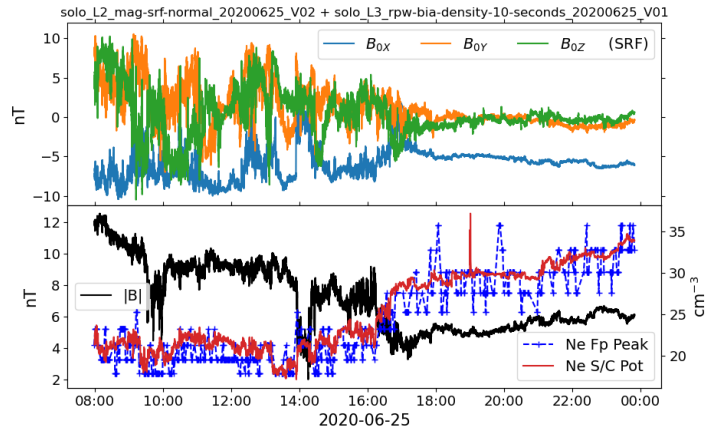
Observations of whistler mode waves by Solar Orbiter's RPW Low Frequency Receiver (LFR): In-flight performance and first results

T. Chust¹ , M. Kretzschmar², D. B. Graham³, O. Le Contel¹, A. Retinò¹, A. Alexandrova¹, M. Berthomier¹,
L. Z. Hadid¹, F. Sahraoui¹, A. Jeandet¹, P. Leroy¹, J.-C. Pellion¹, V. Bouzid¹, B. Katra¹, R. Piberne¹,
Yu. V. Khotyaintsev³, A. Vaivads^{3,4}, V. Krasnoselskikh², J. Souček⁵, O. Santolík^{5,6}, E. Lorfèvre⁷, D. Plettemeier⁸,
M. Steller⁹, Š. Štverák¹⁰, P. Trávníček^{13,10}, A. Vecchio^{11,12}, M. Maksimovic¹¹, S. D. Bale^{13,14,15}, T. S. Horbury¹⁶,
H. O'Brien¹⁶, V. Evans¹⁶, and V. Angelini¹⁶



PSD computed from the snapshots of WF (every 300 s, $\Delta f = 2\text{Hz}$) compared with the PSD computed onboard (every 20 s, $\Delta f = 8$ Hz, BP2 data set)





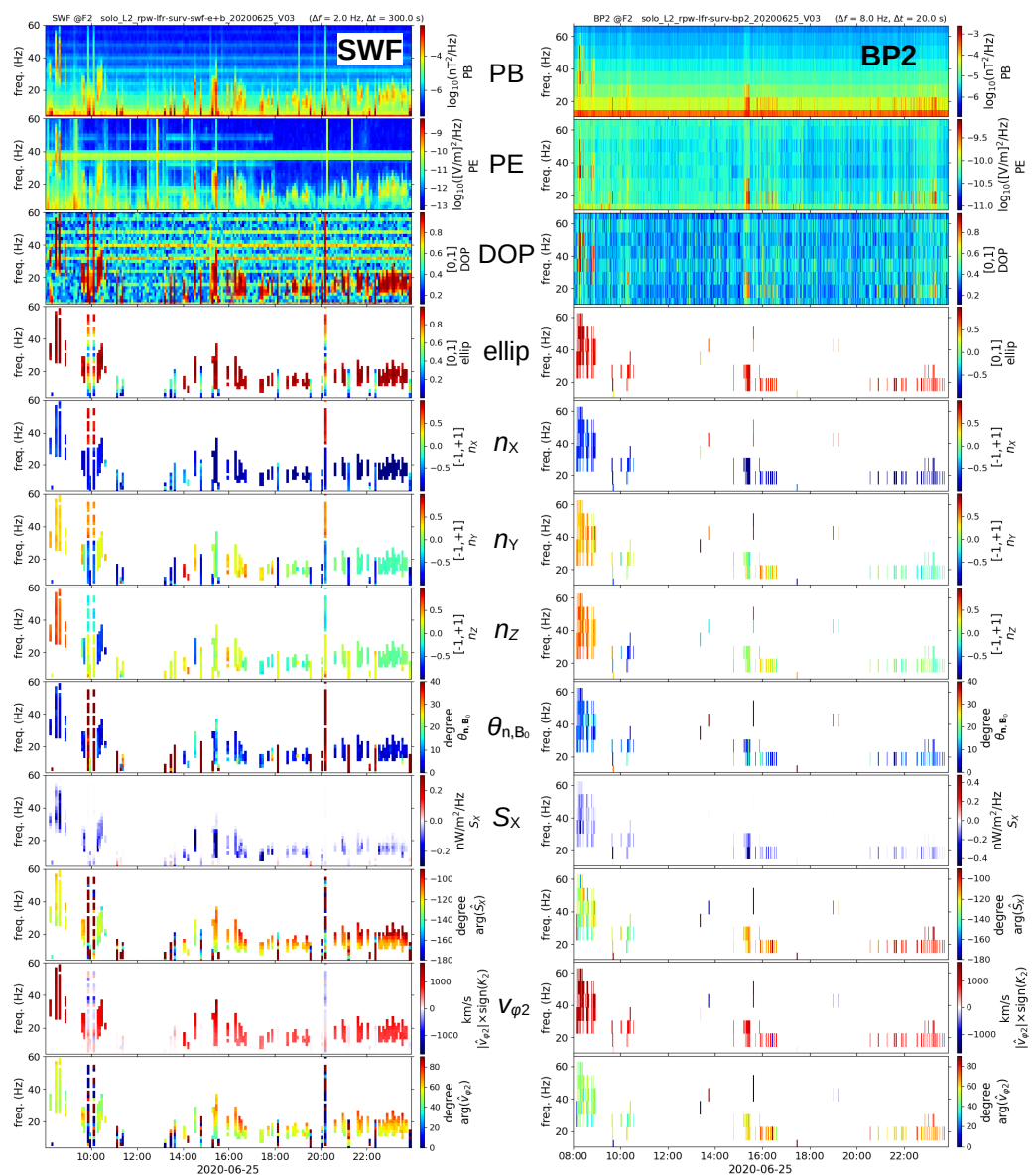
$$\left. \begin{aligned} \mathbf{n} \times \tilde{\mathbf{E}} &= \frac{\omega}{K} \tilde{\mathbf{B}} \\ \tilde{\mathbf{E}} \cdot \mathbf{B}_0 &= 0 \end{aligned} \right\} \Rightarrow \tilde{\mathbf{E}} = -\frac{\omega}{K} \frac{\mathbf{B}_0 \times \tilde{\mathbf{B}}}{\mathbf{n} \cdot \mathbf{B}_0}$$

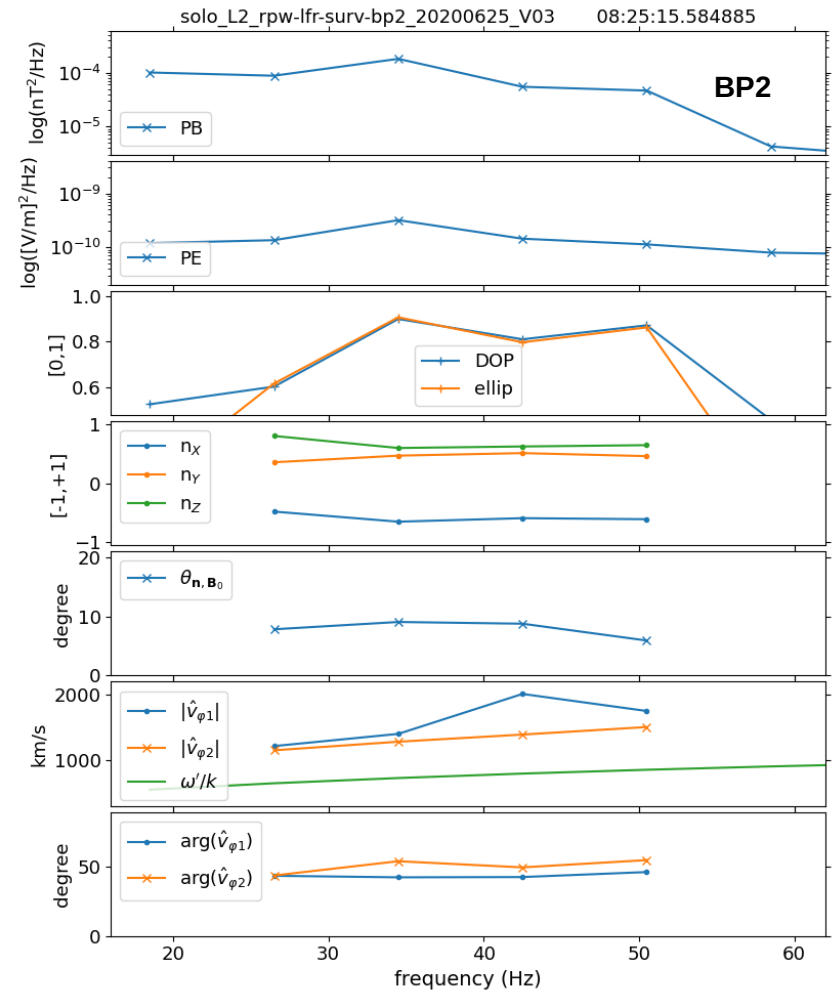
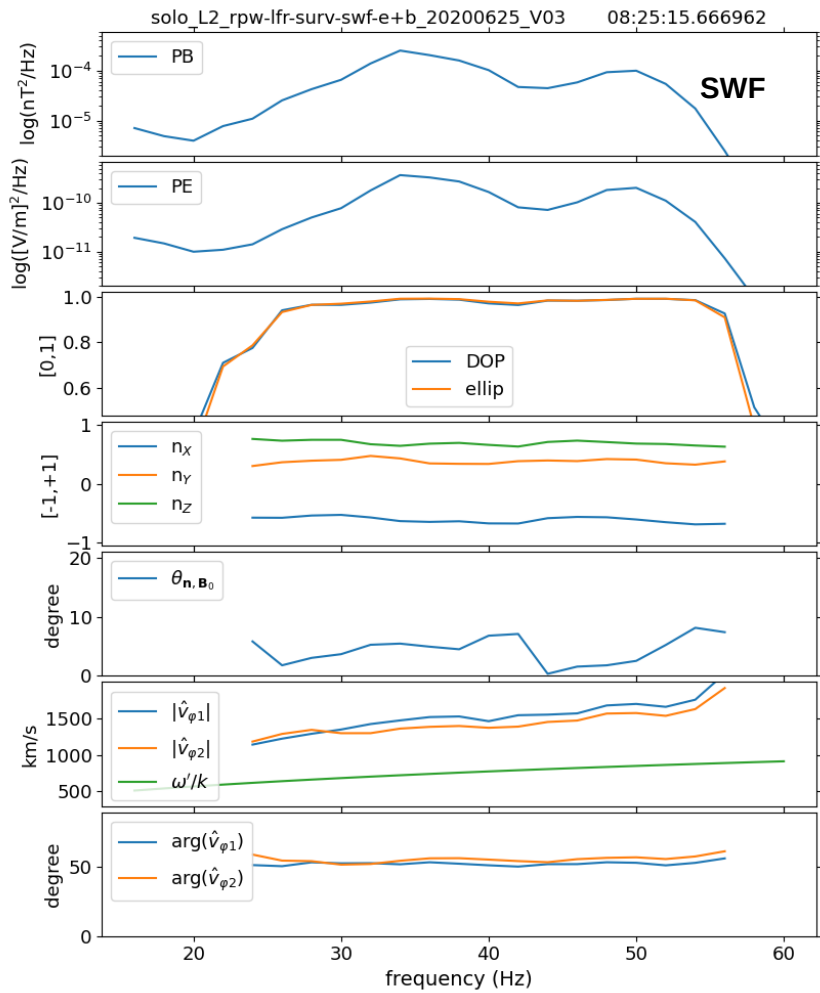
$$\frac{\omega}{K} \approx \frac{(\mathbf{n} \cdot \mathbf{B}_0) \langle \hat{E}_Y \hat{B}_Y^* \rangle_t / \rho_{E_Y B_Y}}{B_{0X} \langle \hat{B}_Z \hat{B}_Y^* \rangle_t / \rho_{B_Z B_Y} - B_{0Z} \langle \hat{B}_X \hat{B}_Y^* \rangle_t / \rho_{B_X B_Y}} = \hat{v}_{\varphi 2}(\omega)$$

with \mathbf{n} , the wave normal vector (Means, JGR, 1972),

and : $\mathbf{k} = \mathbf{n} \times K$

$$\left[\rho_{ij} = \frac{|\langle \hat{P}_i \hat{P}_j^* \rangle_t|}{\sqrt{\langle \hat{P}_i \hat{P}_i^* \rangle_t \langle \hat{P}_j \hat{P}_j^* \rangle_t}} \right]$$

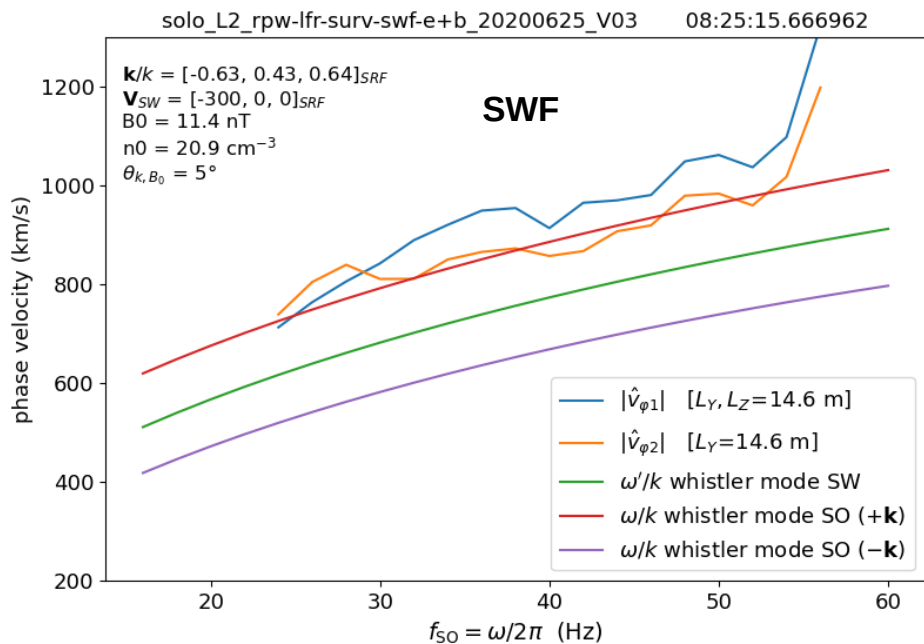




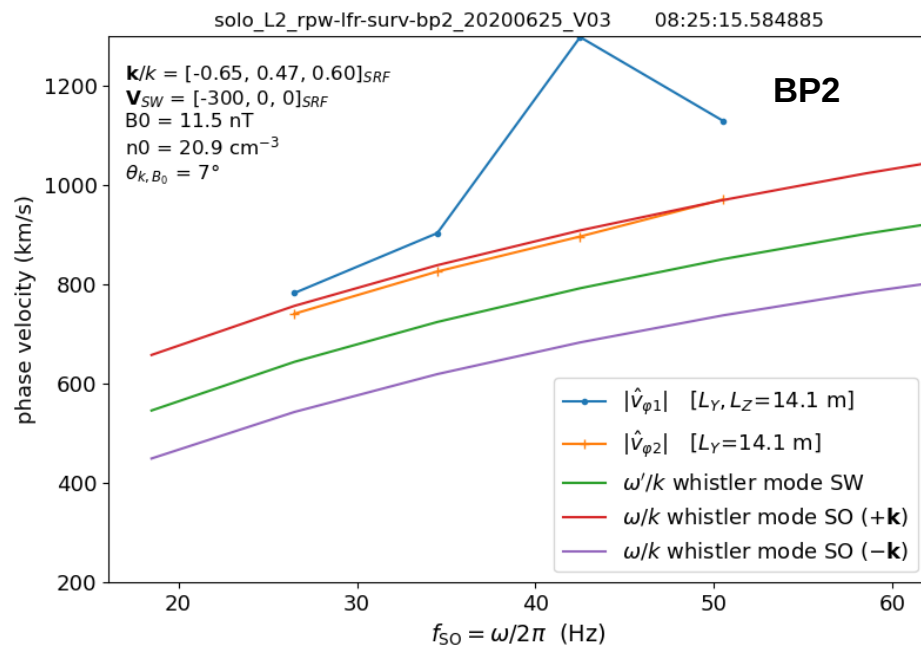
$$\left[\frac{\omega}{K} \approx \frac{n_y \langle \hat{E}_Z \hat{B}_X^* \rangle_t / \rho_{E_Z B_X} - n_z \langle \hat{E}_Y \hat{B}_X^* \rangle_t / \rho_{E_Y B_X}}{\langle \hat{B}_X \hat{B}_X^* \rangle_t} = \hat{v}_{\varphi 1}(\omega) \right]$$

Identification of whistler mode waves in the solar wind

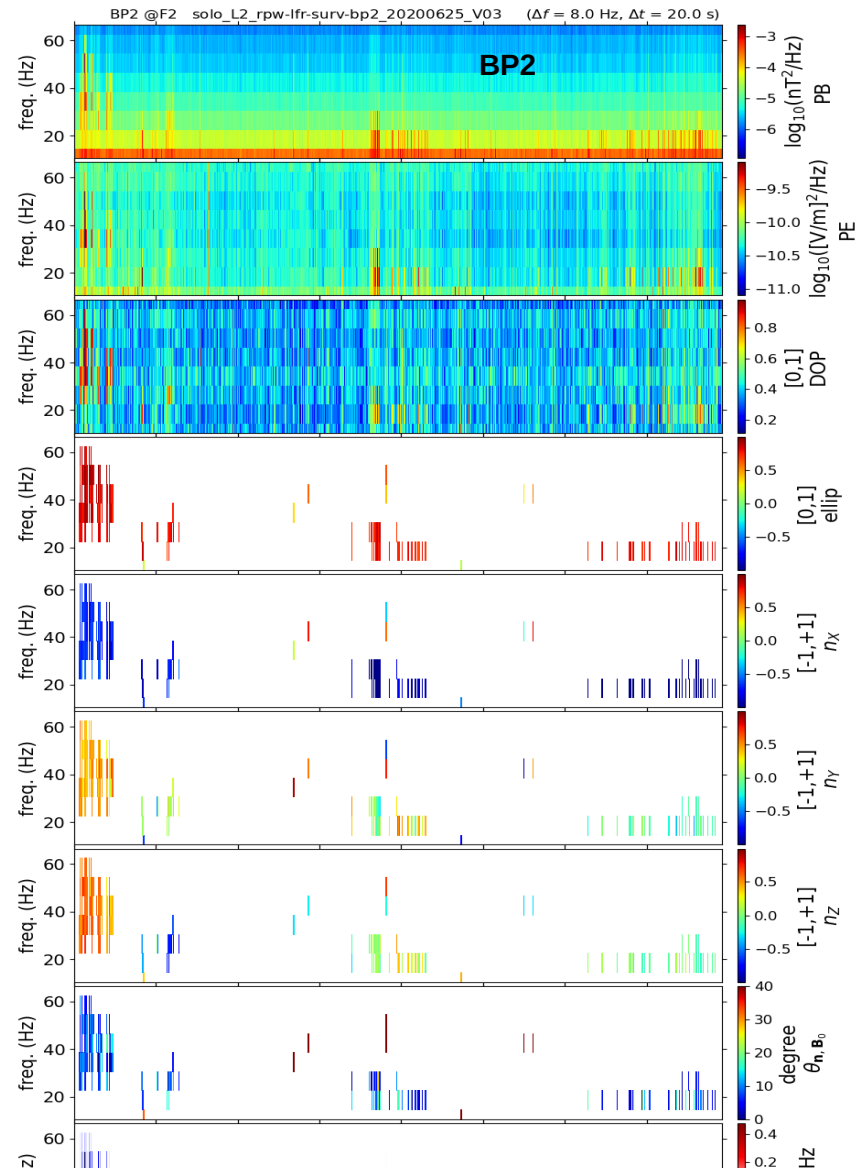
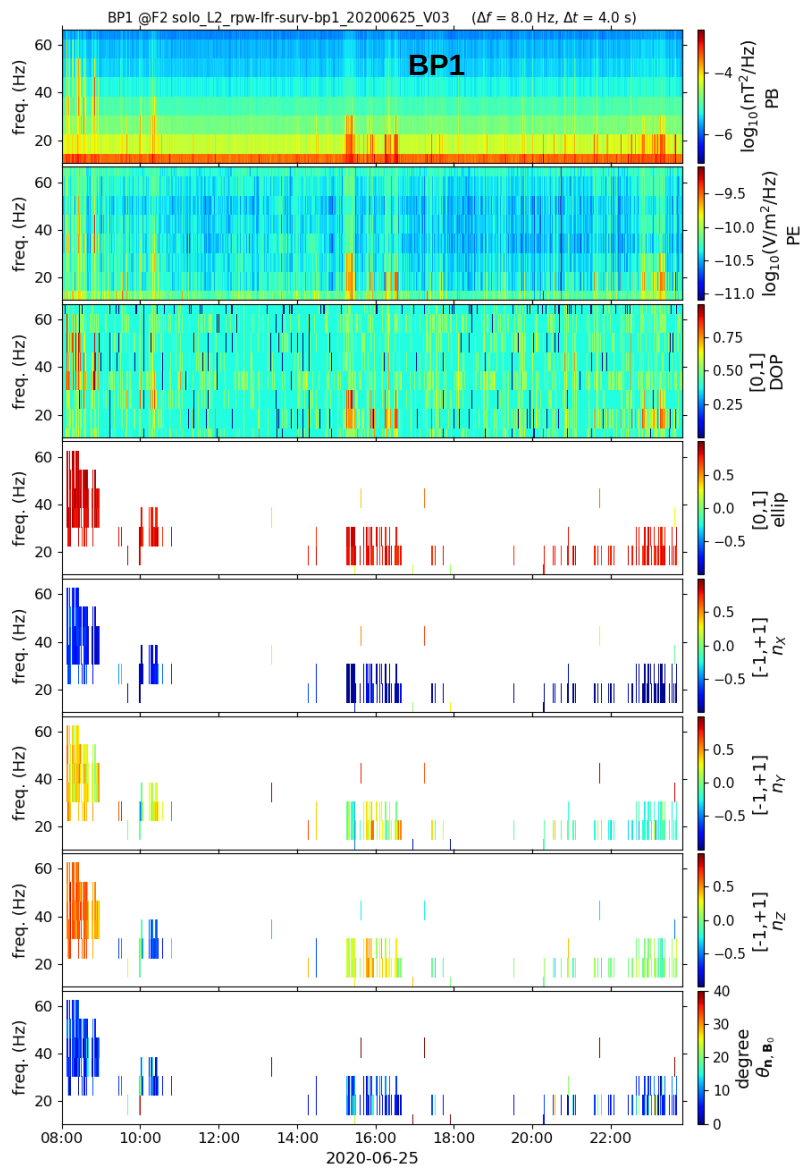
Phase velocity measured (orange) from waveforms (SWF data set) compared with the theoretical (red) Doppler shifted (+ \mathbf{k}) whistler mode



Phase velocity measured (orange) from onboard spectral data products (BP2 data set) compared with the theoretical (red) Doppler shifted (+ \mathbf{k}) whistler mode



$$\left[\omega = \omega' + \mathbf{k} \cdot \mathbf{V}_{SW} \right]$$



Wave parameters computed onboard (every 4 s, $\Delta f = 8$ Hz, BP1 data set) compared with those computed from the BP2 data set (every 20 s, $\Delta f = 8$ Hz)

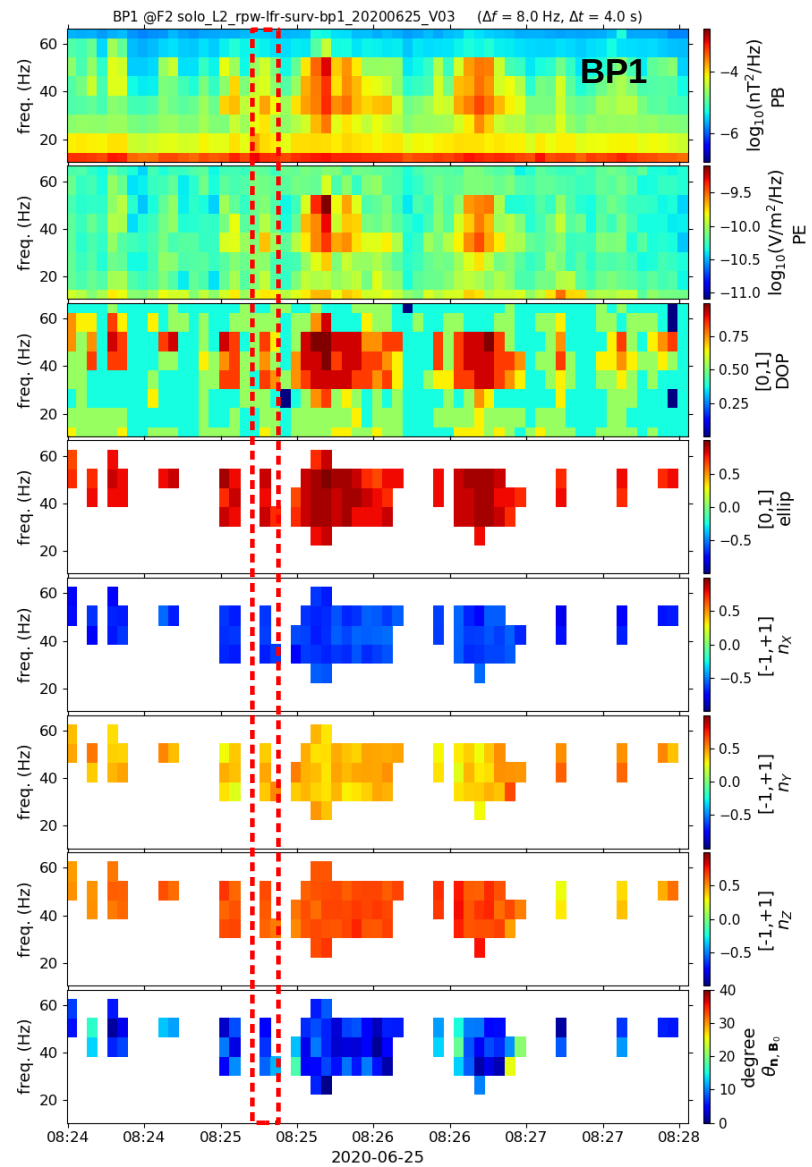
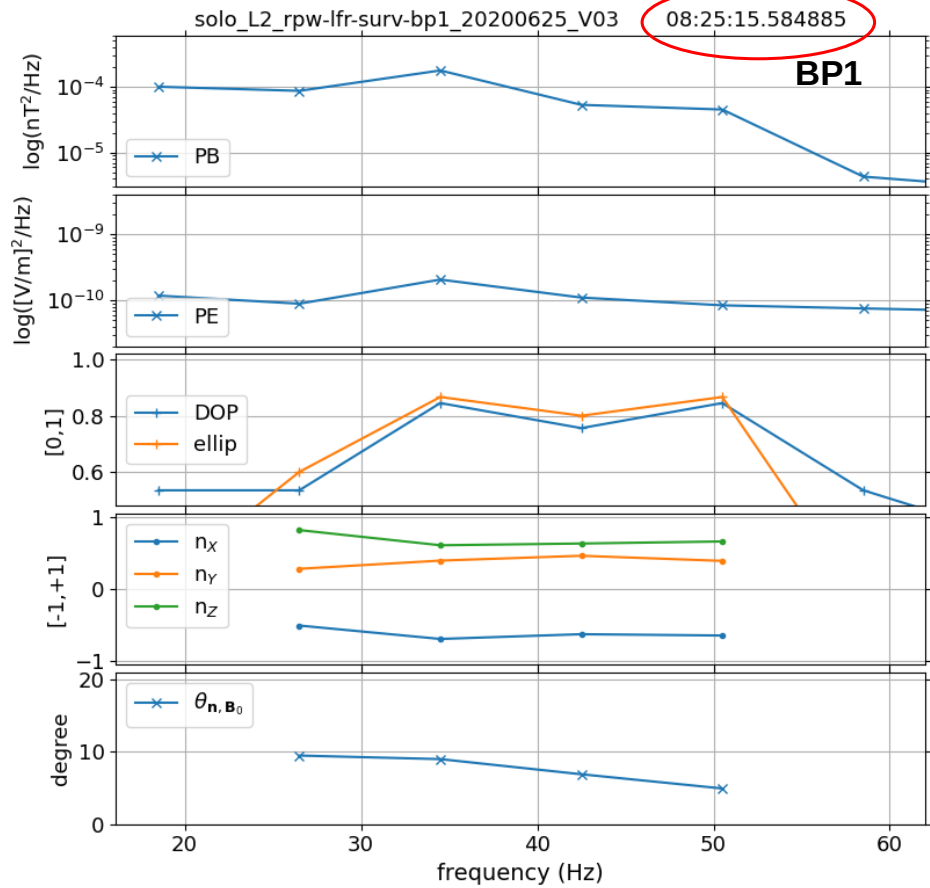
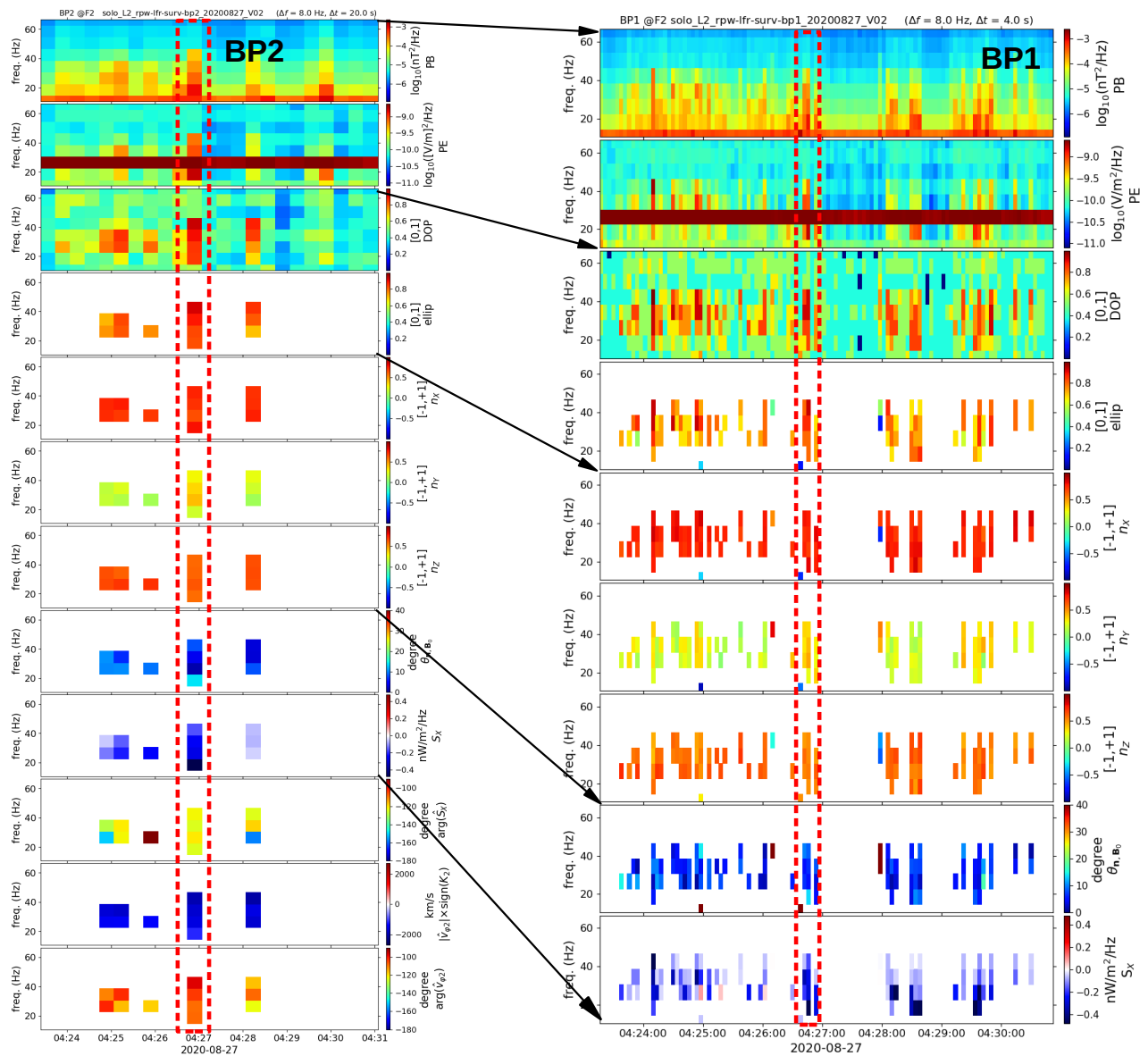


Illustration again of the intermittency of the whistler mode waves and the correct calculation of BP1 data, but this time including the **Poynting flux S_x** , showing that the update of the kcoefficients worked very well

04:26:44 UTC (August 27, 2020)



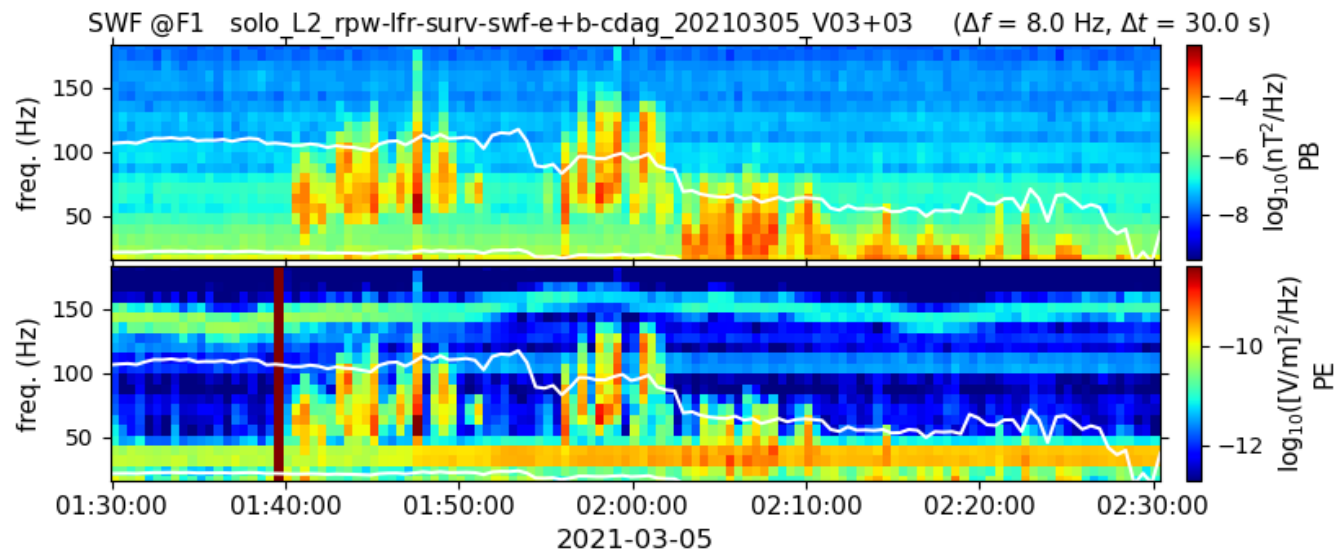
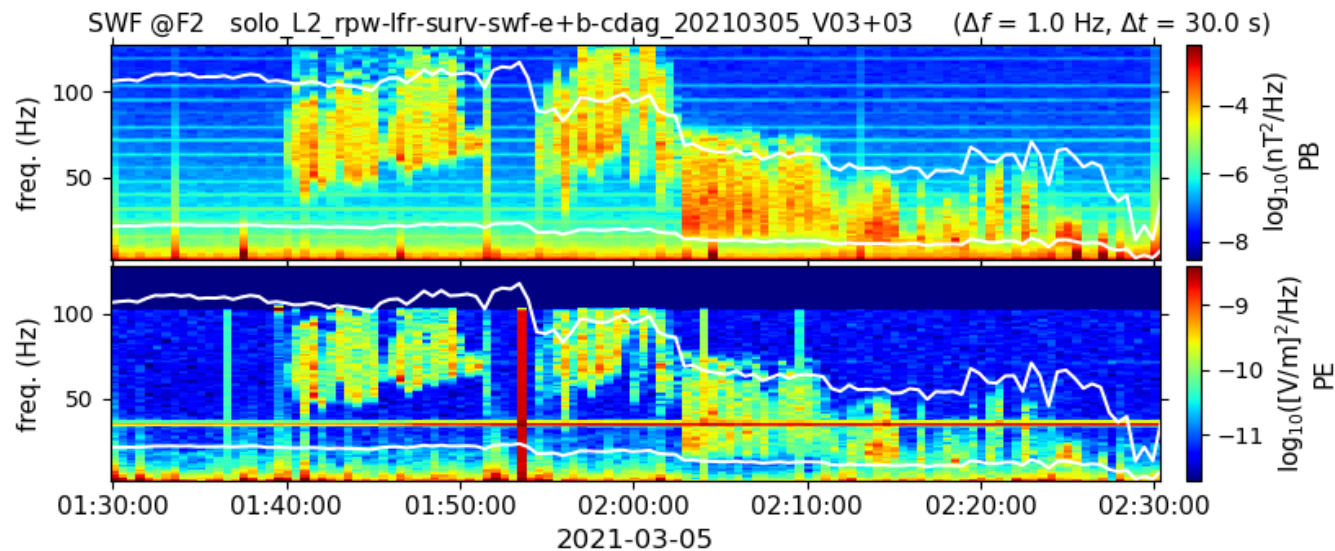
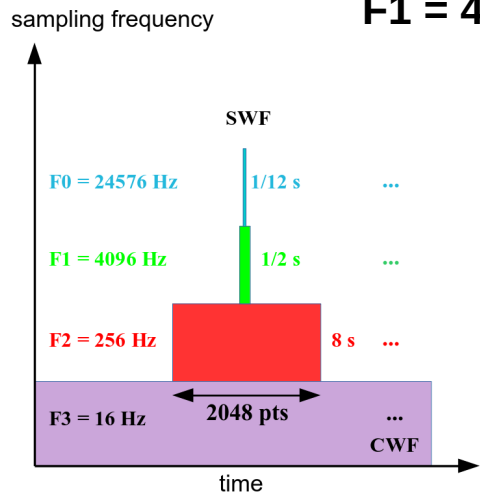
Further verification of the consistency of the LFR data

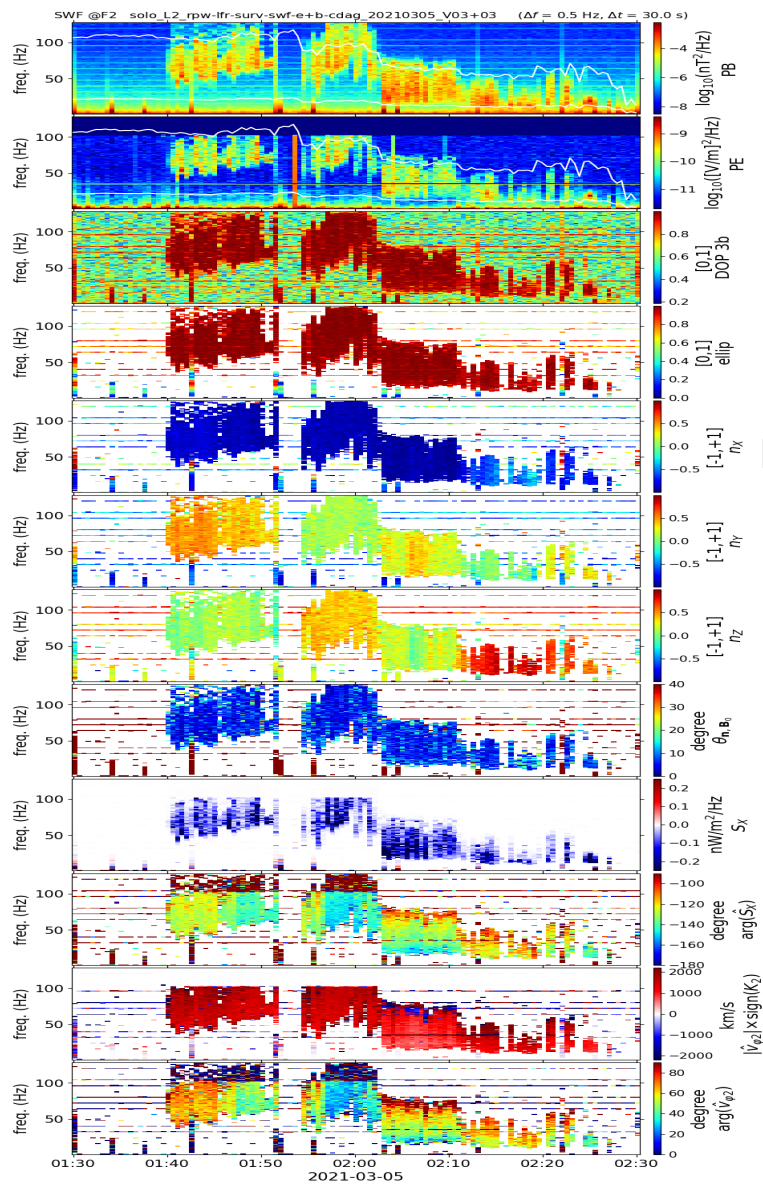
SWF

F2 = 256 Hz

versus

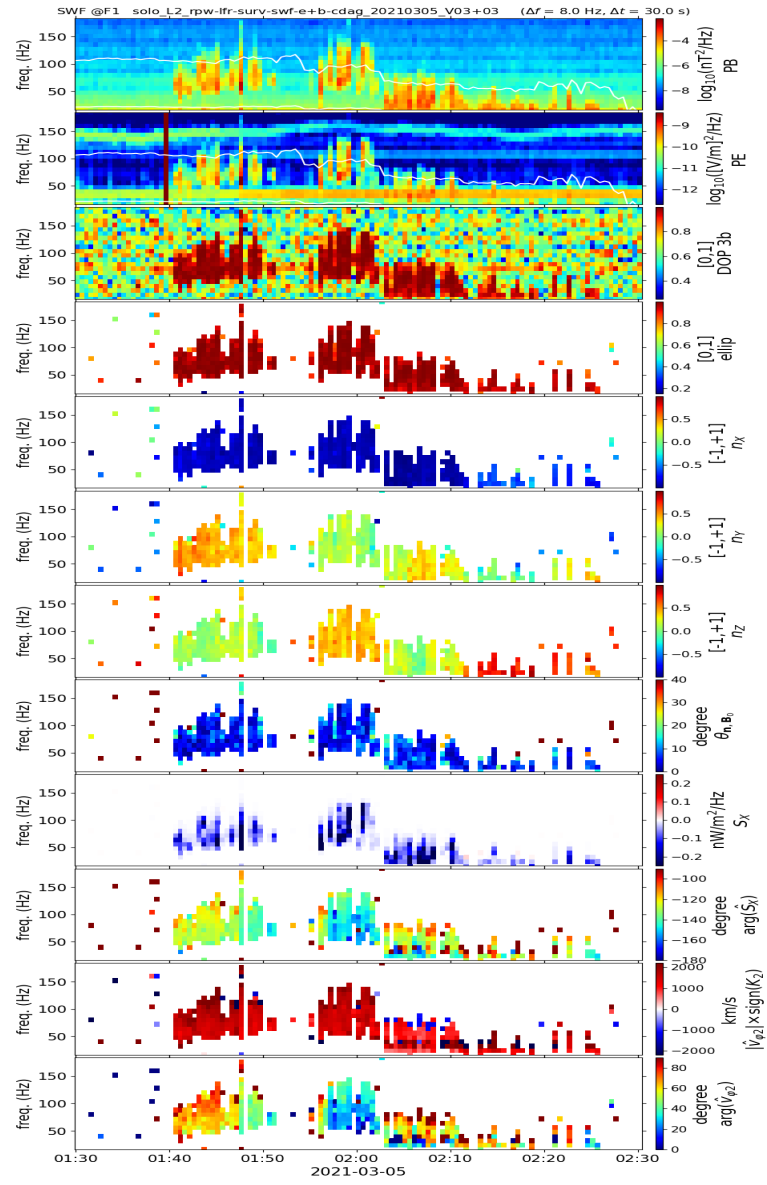
F1 = 4096 Hz

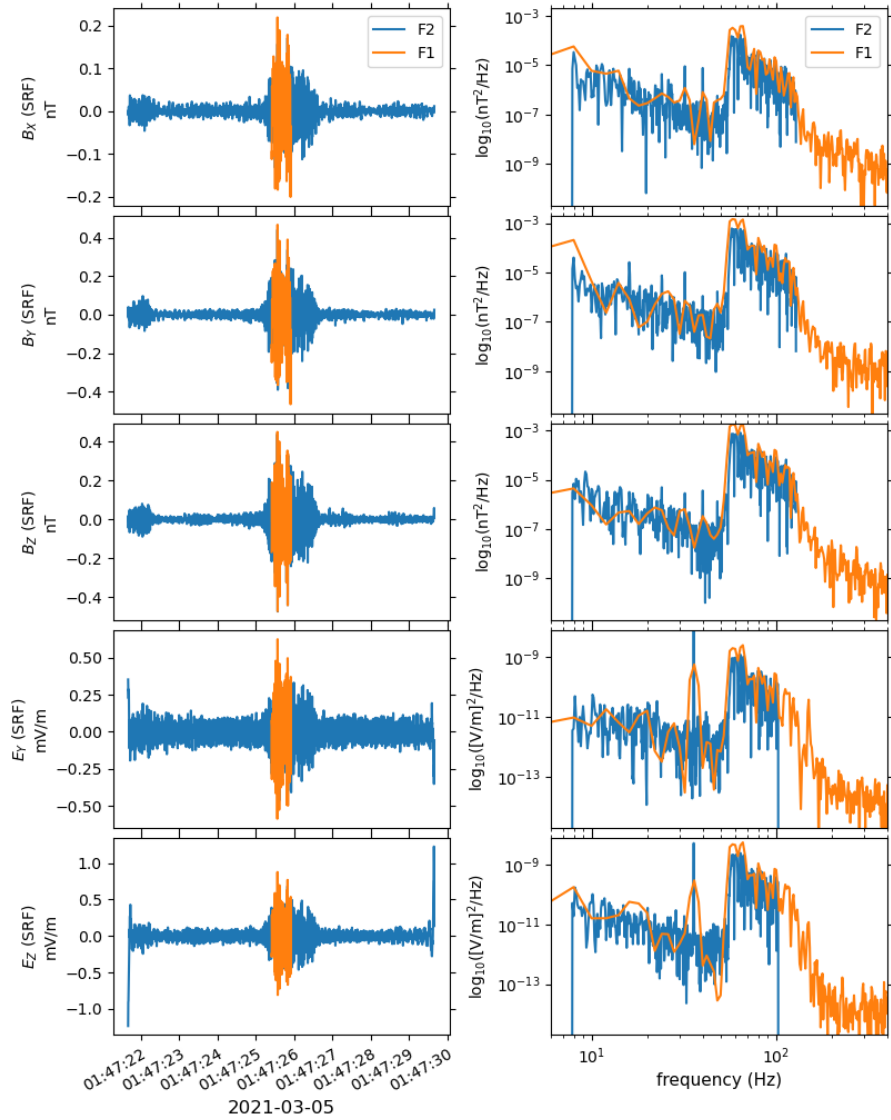




SWF

F2 versus F1

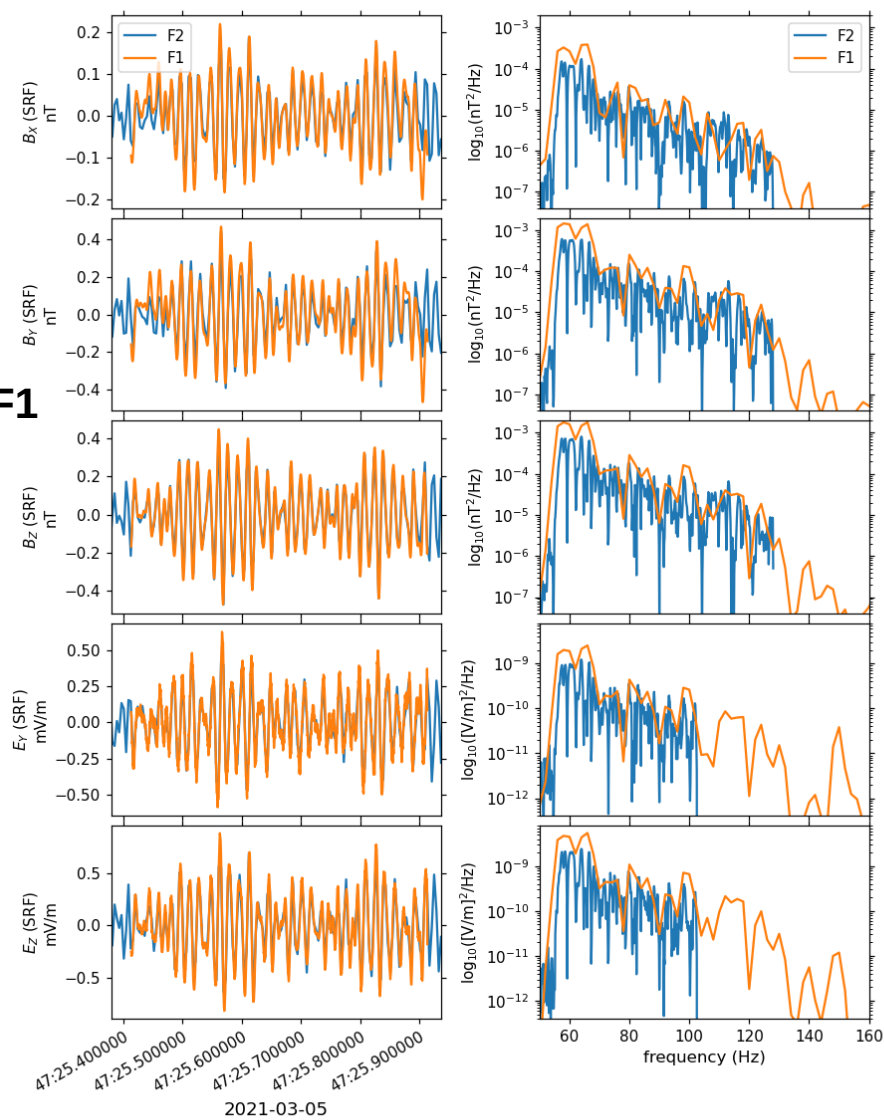


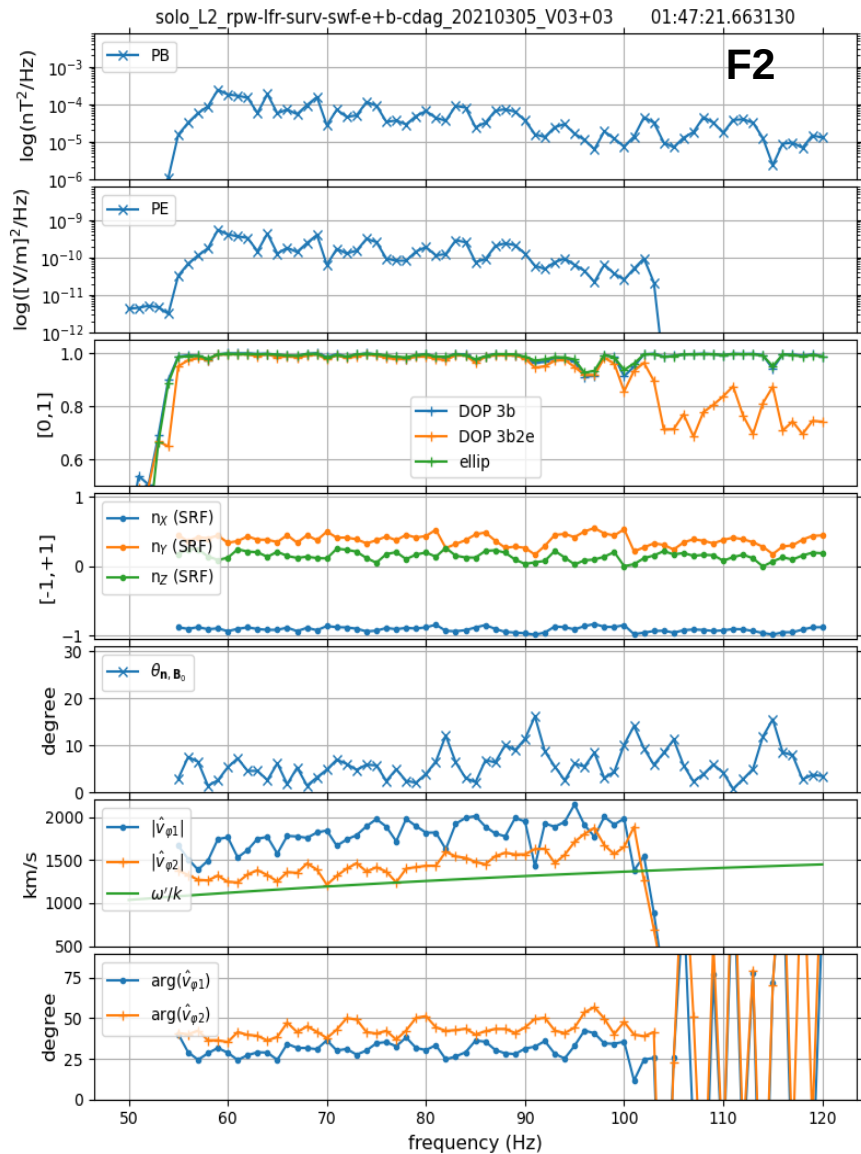


SWF

F2 versus F1

zoom :

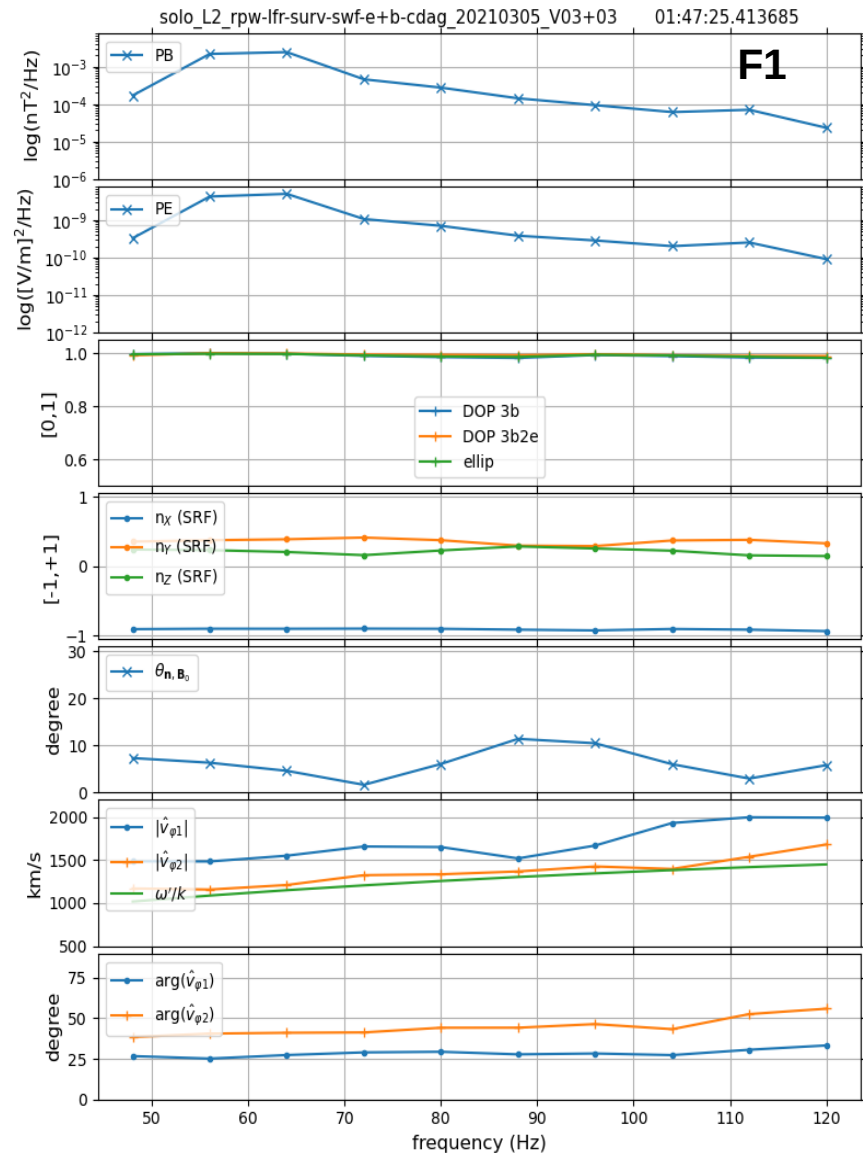


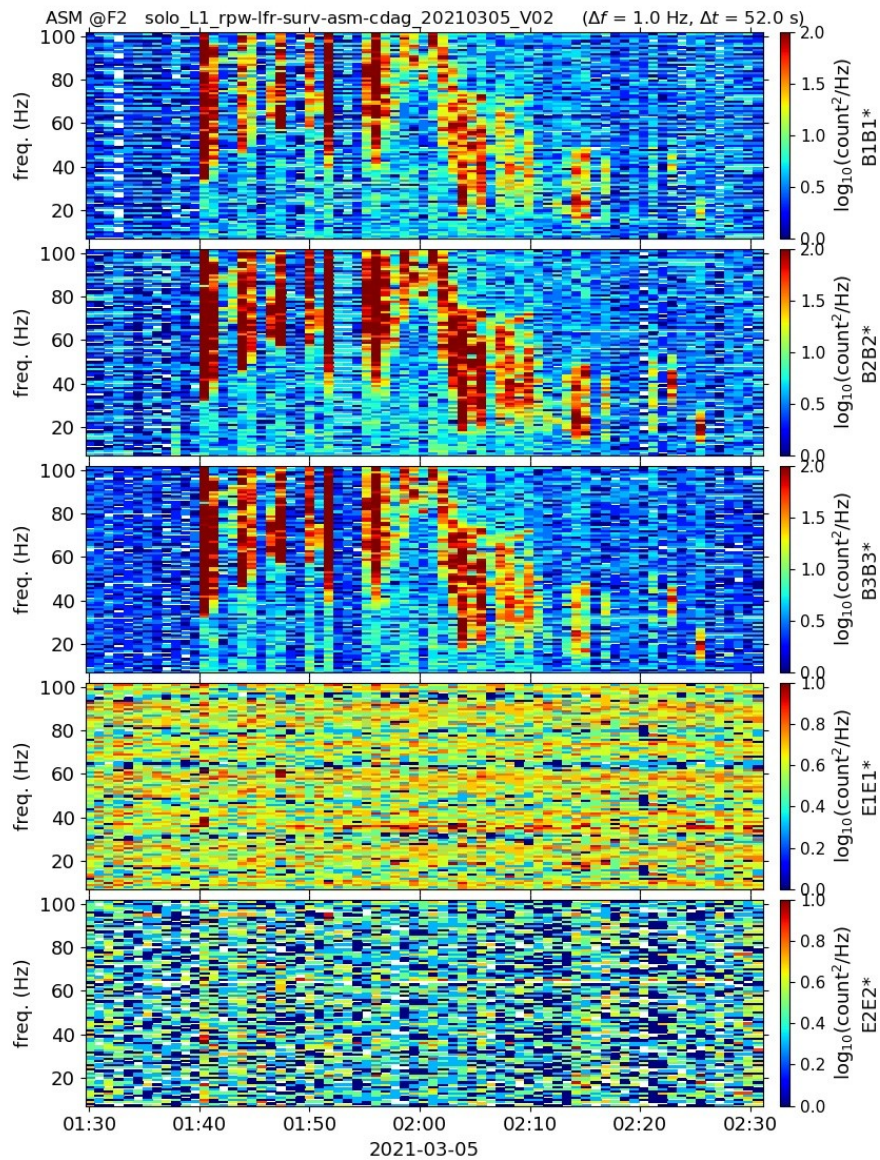


SWF

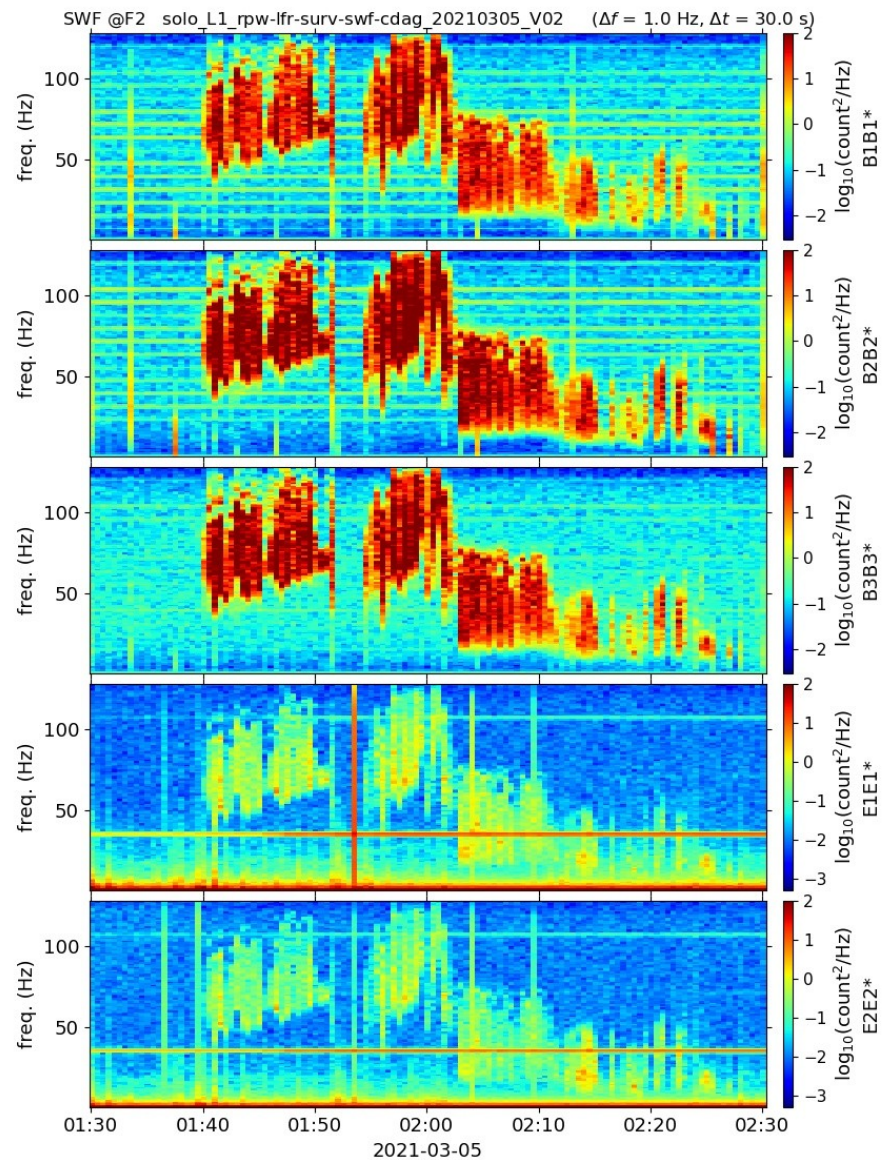
F2 versus F1

Caveat :
 due to the
 intermittency
 features, the
 PSDs show
 differences even
 though the wave
 propagation
 characteristics
 are similar.



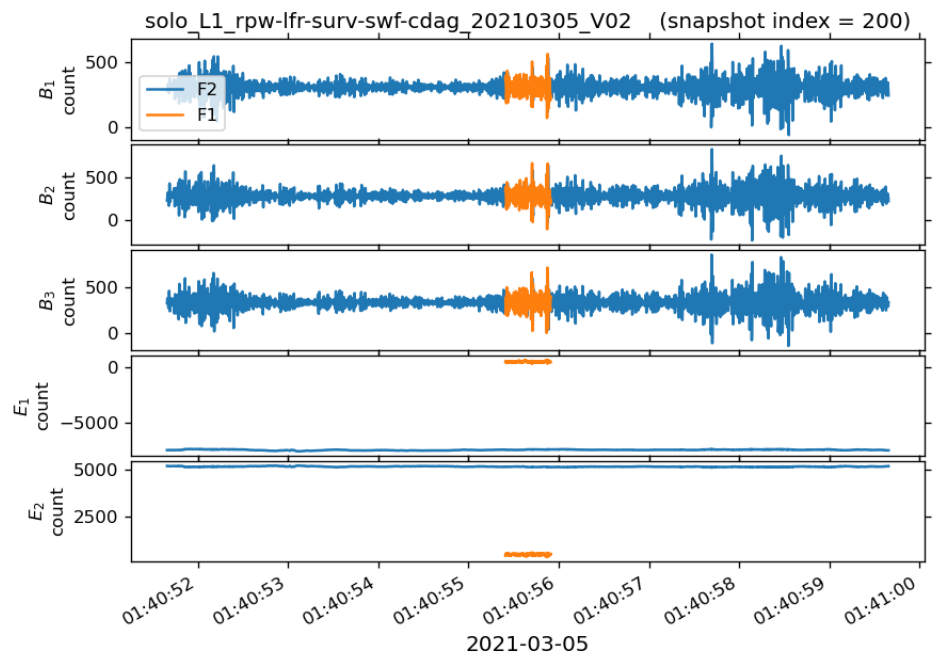
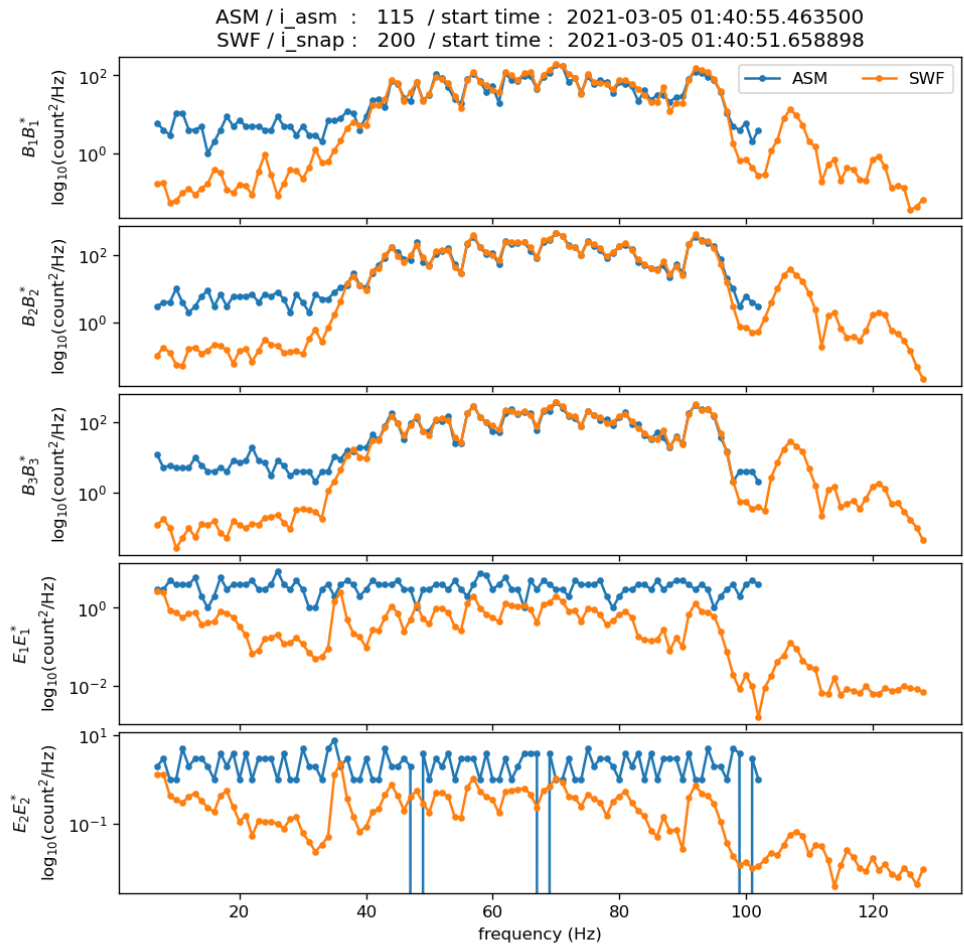
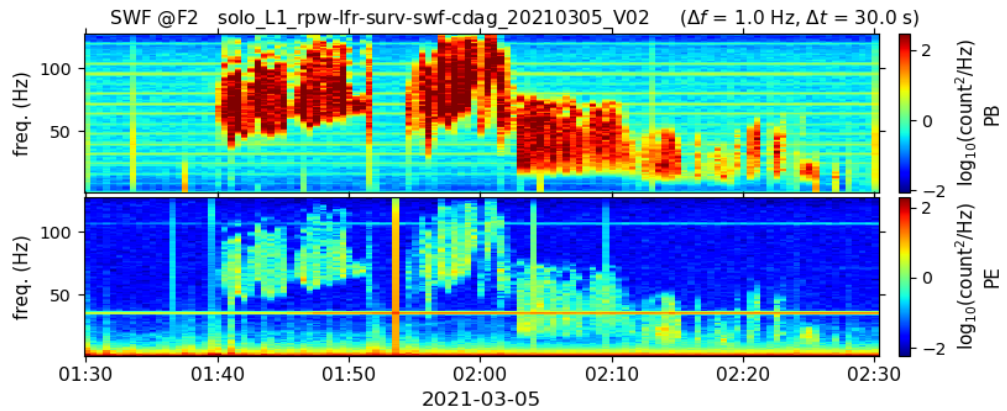


F2
ASM
versus
SWF



F2

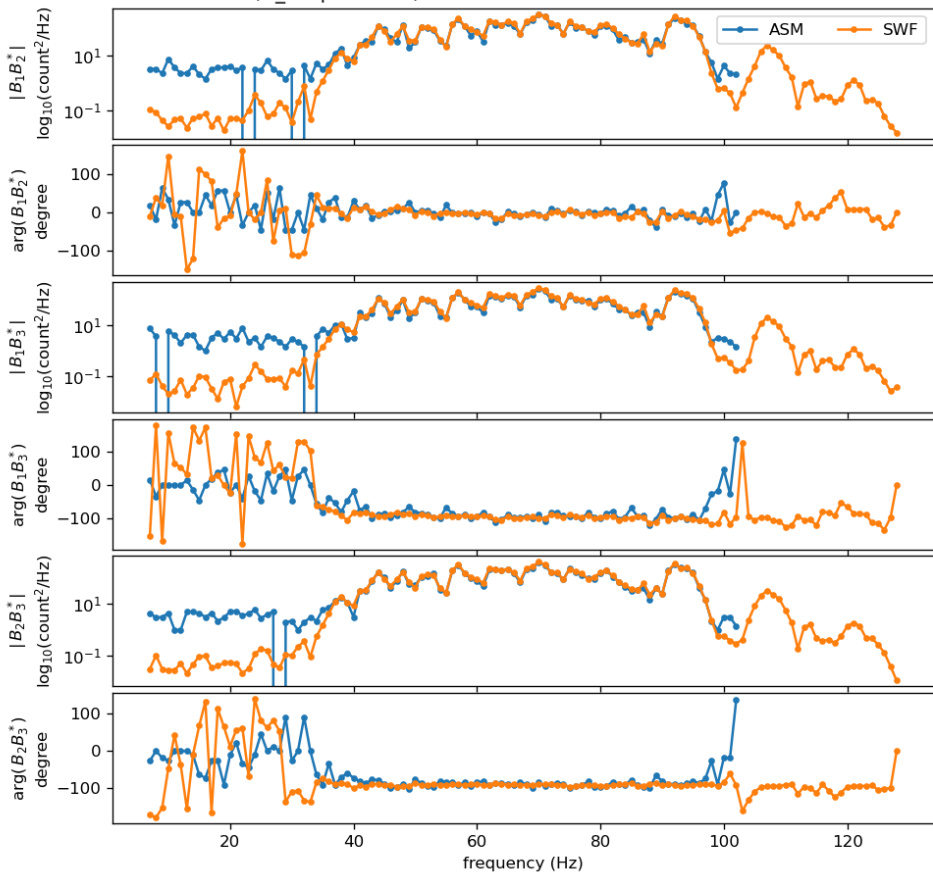
ASM versus SWF



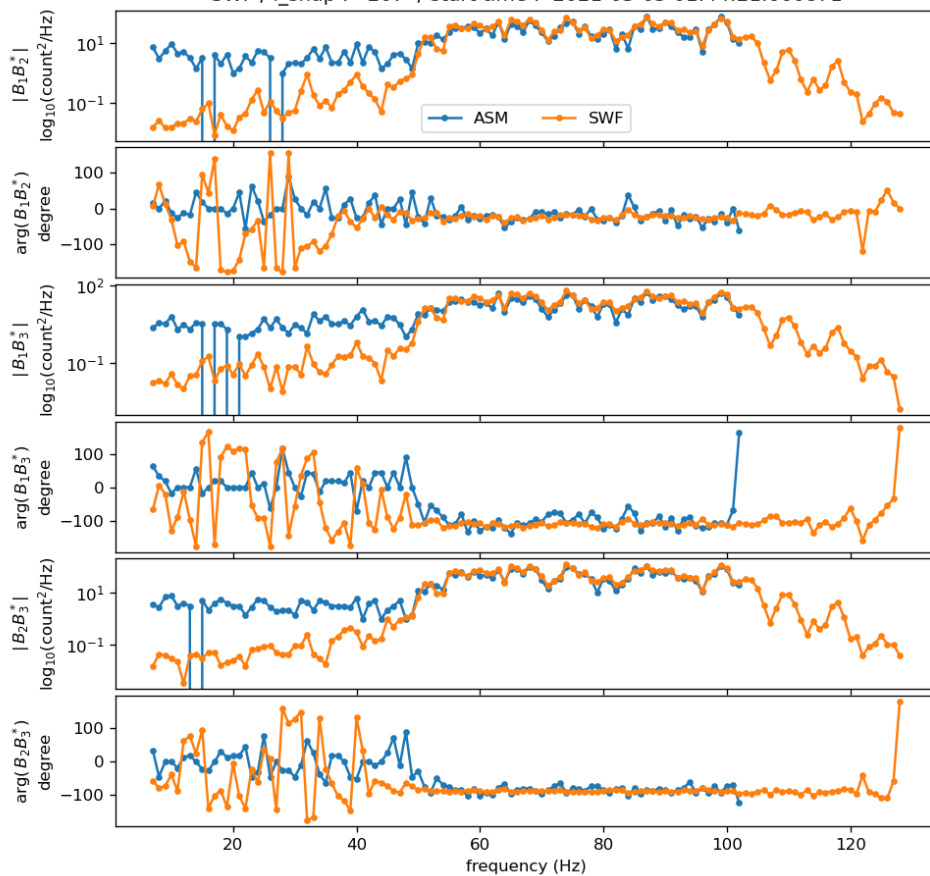
ASM versus SWF

F2

ASM / i_asm : 115 / start time : 2021-03-05 01:40:55.463500
SWF / i_snap : 200 / start time : 2021-03-05 01:40:51.658898



ASM / i_asm : 119 / start time : 2021-03-05 01:44:23.461579
SWF / i_snap : 207 / start time : 2021-03-05 01:44:21.660871



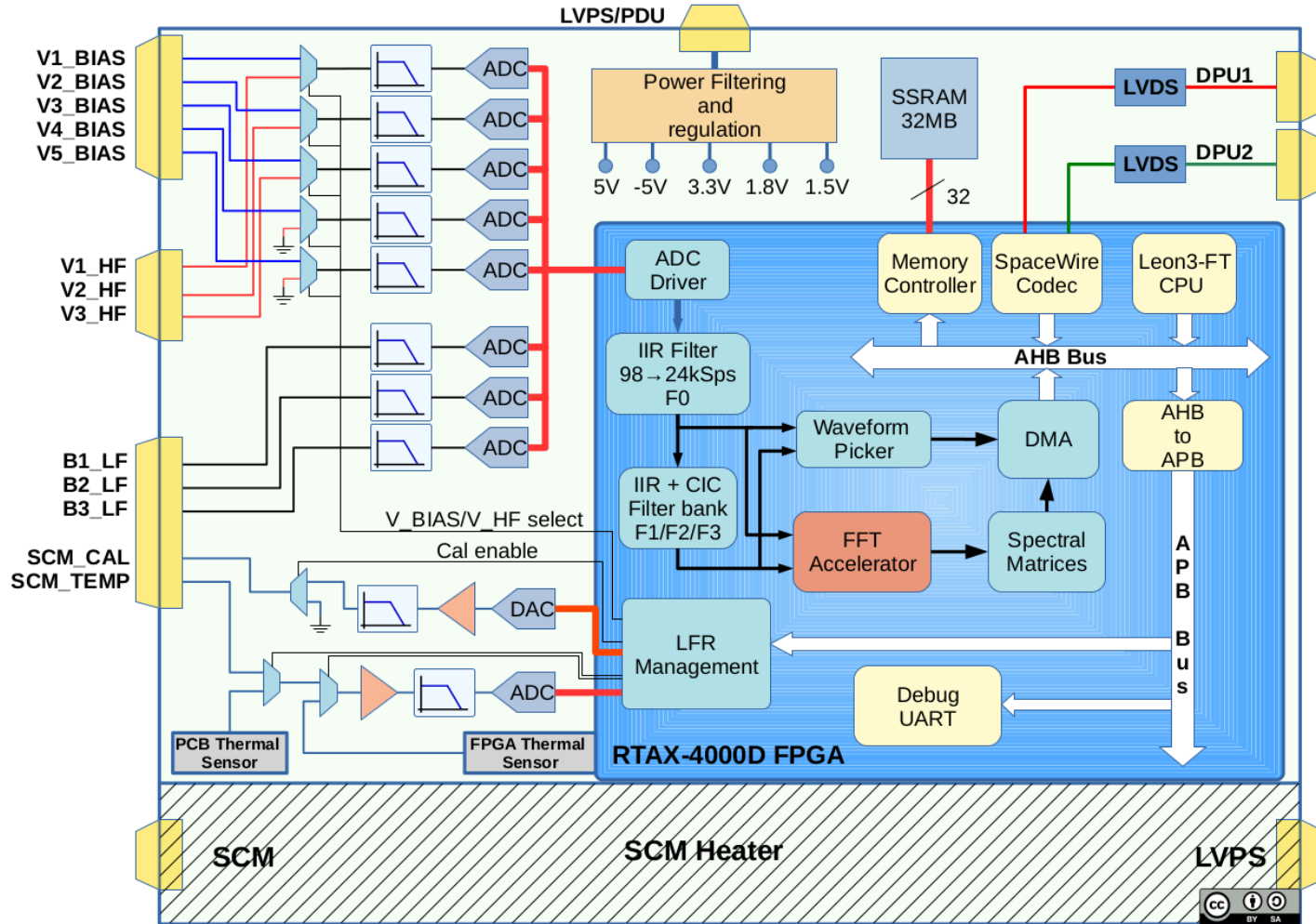
Conclusion

- Where possible, comparisons between all LFR data products show a **very good consistency**
- So far, **phase shift issue (between E and B) can be neglected** when determining the sign of S_x or the direction of the wave propagation (Kretzschmar et al. 2021; Chust et al. 2021).
- **Fluctuations in the determination of the effective antenna lengths** are still not well understood (Steinvall et al. 2021; Kretzschmar et al. 2021; Chust et al. 2021).

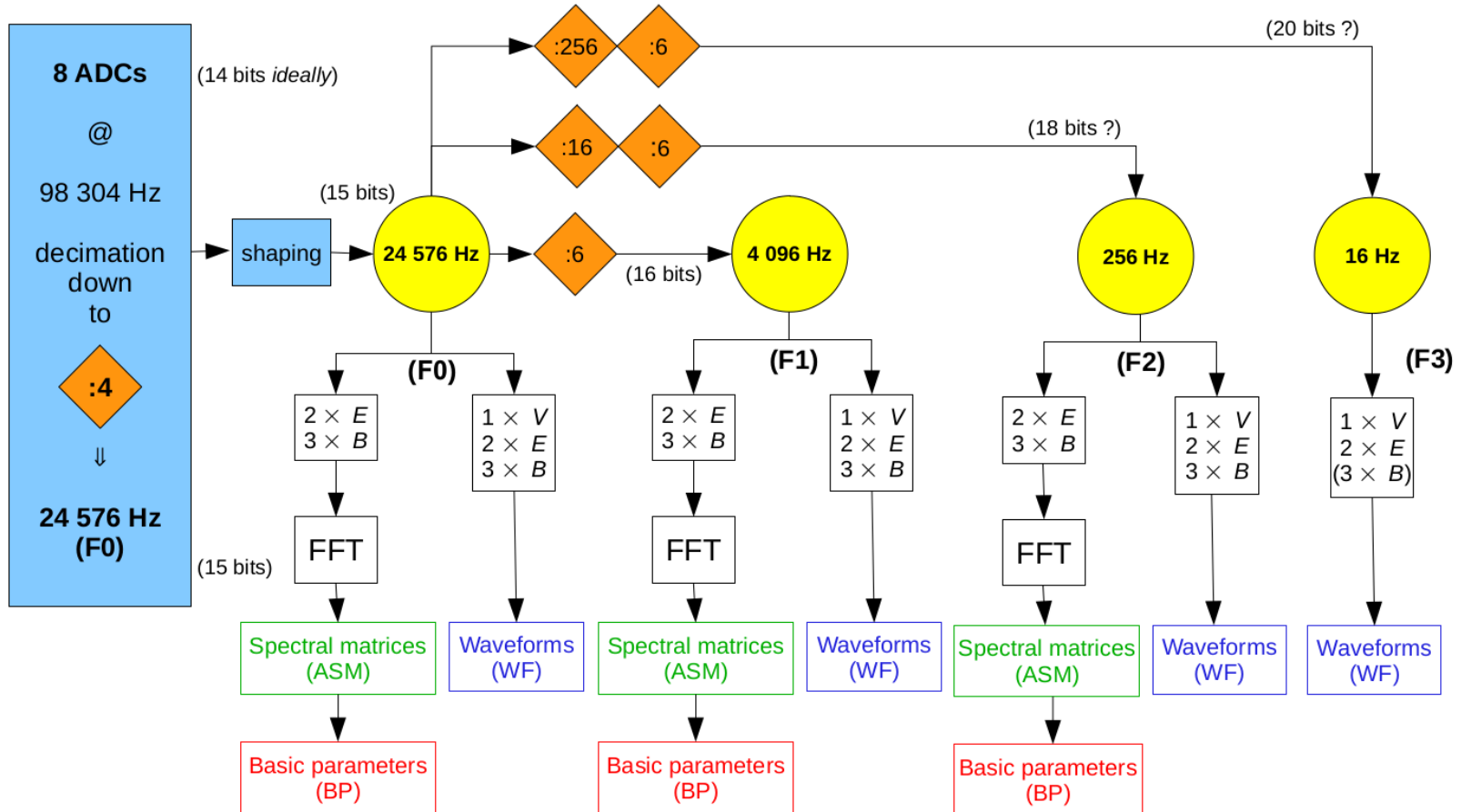


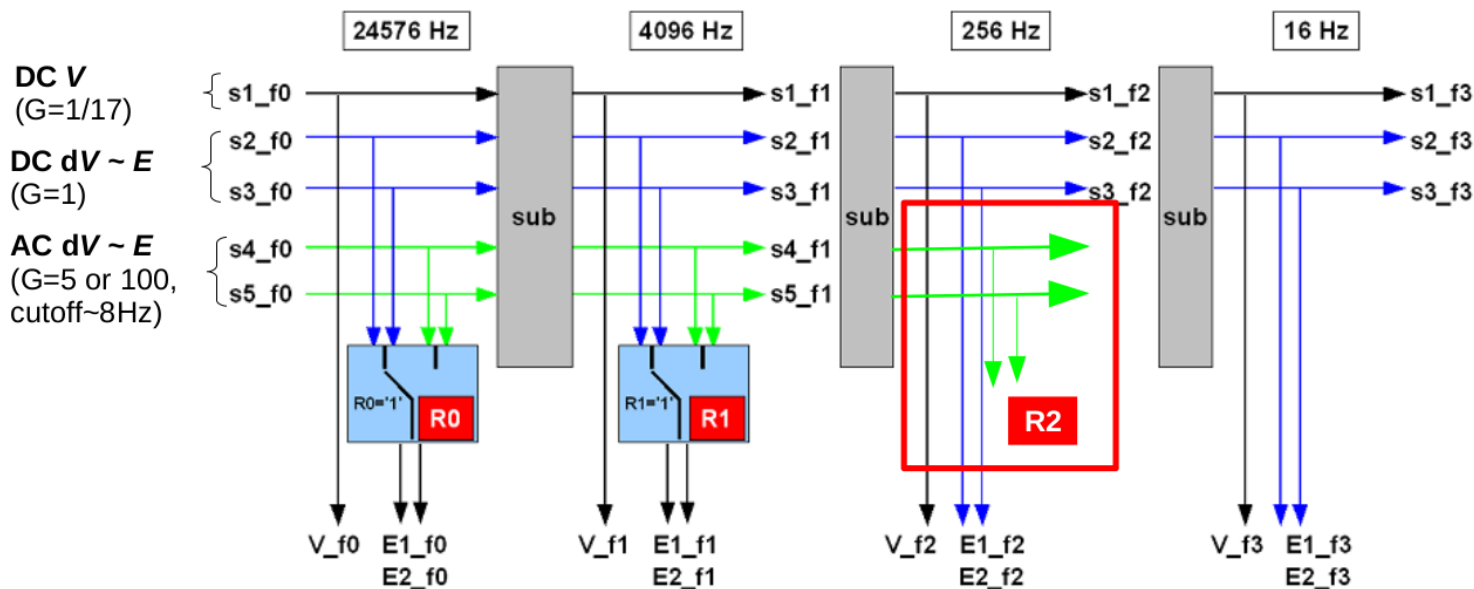
Additional slides

LFR block diagram



LFR Decimation and Processing Strategy





LFR current set of Basic Parameters

“Instantaneous” 5 x 5 spectral matrix
(256-point FFT)

$$\mathbf{SM}(\omega_j^{(m)}) = \begin{bmatrix} B_1 B_1^* & B_1 B_2^* & B_1 B_3^* & B_1 E_1^* & B_1 E_2^* \\ cc & B_2 B_2^* & B_2 B_3^* & B_2 E_1^* & B_2 E_2^* \\ cc & cc & B_3 B_3^* & B_3 E_1^* & B_3 E_2^* \\ cc & cc & cc & E_1 E_1^* & E_1 E_2^* \\ cc & cc & cc & cc & E_2 E_2^* \end{bmatrix}$$

$m = 0, 1, 2$
for F0, F1, F2

Time Averaged Spectral Matrix (ASM)

$$\mathbf{ASM}(\omega_j^{(m)}) = \frac{1}{N_{SM}^{(m)}} \sum_{k=1}^{N_{SM}^{(m)}} \mathbf{SM}_k(\omega_j^{(m)}) = \langle \mathbf{SM} \rangle_{time}$$

Frequency average ...

$$\mathbf{S}(\omega_j^{(m)}) = \langle \mathbf{ASM} \rangle_{frequency}$$

... before computations of the BPs
(i.e. wave parameters)

Mono-**k**

assumption: (Means, JGR, 1972) {
(Samson & Olson, GJRA, 1980) {

$$\mathbf{n} \times \mathbf{E} = \frac{\omega}{k} \mathbf{B} \longrightarrow$$

$$\frac{S_{ij}}{\sqrt{S_{ii} S_{jj}}} \longrightarrow$$

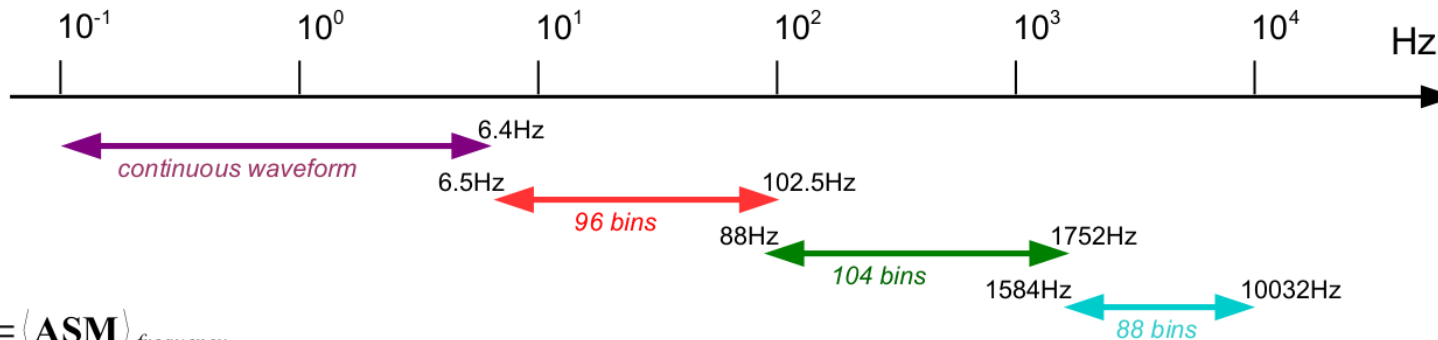
- BP1 PB: Power spectrum of the magnetic field (**B**)
- BP1 PE: Power spectrum of the electric field (**E**) => kcoef
- BP1 NVEC: Wave normal vector (from **B**)
- BP1 ELLIP: Wave ellipticity estimator (from **B**)
- BP1 DOP: Wave planarity estimator (from **B**)
- BP1 SX: X_{SRF} (radial)-component of the Poynting vector => kcoef
- BP1 VPHI: Phase velocity estimator => kcoef (patch needed)
- BP2 AUTO: Autocorrelations
- BP2 CROSS: Normalized cross correlations

- (1) Depending on the frequency channel, **selection** of 96, 104 or 88 consecutive **frequency bins** among 128 ($N_{FFT} = 256$) of the *time* averaged spectral matrices.
- (2) Then, the ASMs are averaged over packets of N_{freq} (8 or 4) consecutive bins :

$$\Delta f^{(m)} = \frac{f_m}{N_{FFT}} \times N_{freq}$$

$N_{freq} = 8$

$f_3 = 16 \text{ Hz}$	=> waveform	[DC, 8Hz]		$f_3 / 2.5 = 6.4 \text{ Hz}$
$f_2 = 256 \text{ Hz}$	=> 12 frequencies	[6.5Hz, 102.5Hz]	$\Delta f^{(2)} = 8 \text{ Hz}$	$f_2 / 2.5 = 102.4 \text{ Hz}$
$f_1 = 4096 \text{ Hz}$	=> 13 frequencies	[88Hz, 1752Hz]	$\Delta f^{(1)} = 128 \text{ Hz}$	$f_1 / 2.5 = 1638.4 \text{ Hz}$
$f_0 = 24576 \text{ Hz}$	=> 11 frequencies	[1584Hz, 10032Hz]	$\Delta f^{(0)} = 768 \text{ Hz}$	$f_0 / 2.5 = 9830.4 \text{ Hz}$



$$\mathbf{S} = \langle \mathbf{ASM} \rangle_{frequency}$$

Computation of the k-coefficients for PE

Power spectrum of the electric field

$$\begin{aligned} \langle E_{Y'} E_{Y'}^* + E_{Z'} E_{Z'}^* \rangle &= \left\langle \mathbf{E}_{ANT}^T \cdot \frac{1}{|A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}|^2} \begin{bmatrix} |A_{2Y'}|^2 + |A_{2Z'}|^2 & -A_{1Y'}^* A_{2Y'} - A_{1Z'}^* A_{2Z'} \\ -A_{1Y'} A_{2Y'}^* - A_{1Z'} A_{2Z'}^* & |A_{1Y'}|^2 + |A_{1Z'}|^2 \end{bmatrix} \cdot \mathbf{E}_{ANT}^* \right\} \\ &= \frac{|A_{2Y'}|^2 + |A_{2Z'}|^2}{|A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}|^2} \left(S_{44} + \frac{|A_{1Y'}|^2 + |A_{1Z'}|^2}{|A_{2Y'}|^2 + |A_{2Z'}|^2} S_{55} - 2 \Re \left[\frac{A_{1Y'}^* A_{2Y'} + A_{1Z'}^* A_{2Z'}}{|A_{2Y'}|^2 + |A_{2Z'}|^2} S_{45} \right] \right) \end{aligned}$$

Calibration factor



$$PE = S_{44} k_{44}^{pe} + S_{55} k_{55}^{pe} + \Re [S_{45} k_{45}^{pe}]$$

$$\text{with } \begin{cases} k_{44}^{pe} = 1 \\ k_{55}^{pe} = \frac{|A_{1Y'}|^2 + |A_{1Z'}|^2}{|A_{2Y'}|^2 + |A_{2Z'}|^2} \\ k_{45}^{pe} = -2 \frac{A_{1Y'}^* A_{2Y'} + A_{1Z'}^* A_{2Z'}}{|A_{2Y'}|^2 + |A_{2Z'}|^2} \end{cases}$$

WARNING: The TF of BIAS and LFR are implicitly embodied in the TF matrix of ANT (just a common calibration factor)

X_{SRF} -component of the Poynting vector

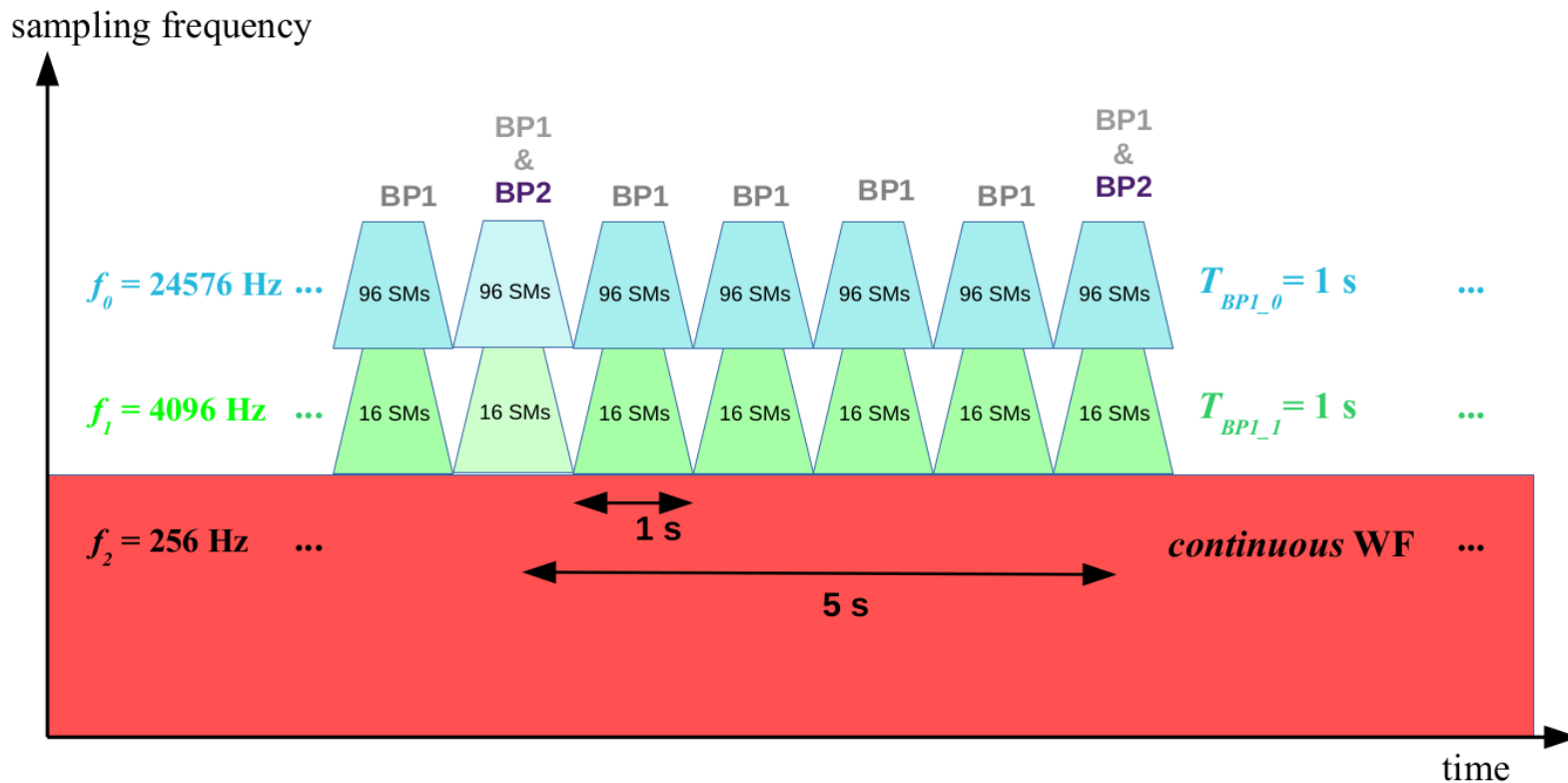
$$\begin{aligned}
 \langle S_{X'} \rangle &= \langle (\mathbf{E} \times \mathbf{B}^*)_{X'} \rangle = \langle E_{Y'} B_{Z'}^* \rangle - \langle E_{Z'} B_{Y'}^* \rangle \\
 &= \left\langle \frac{A_{2Z'} E_1 - A_{1Z'} E_2}{A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}} \frac{1}{C_{1Y}^*} \tilde{m}_{Z'j}^* B_j^* \right\rangle - \left\langle \frac{-A_{2Y'} E_1 + A_{1Y'} E_2}{A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}} \frac{1}{C_{1Y}^*} \tilde{m}_{Y'j}^* B_j^* \right\rangle \\
 &= \frac{(A_{2Y'} \tilde{m}_{Y'j}^* + A_{2Z'} \tilde{m}_{Z'j}^*) \langle E_1 B_j^* \rangle - (A_{1Y'} \tilde{m}_{Y'j}^* + A_{1Z'} \tilde{m}_{Z'j}^*) \langle E_2 B_j^* \rangle}{(A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}) C_{1Y}^*} \\
 &= \underbrace{\frac{\sqrt{|A_{2Y'}|^2 + |A_{2Z'}|^2}}{(A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}) C_{1Y}^*}}_{\text{Calibration factor}} \left[\frac{A_{2Y'} \tilde{m}_{Y'j}^* + A_{2Z'} \tilde{m}_{Z'j}^*}{\sqrt{|A_{2Y'}|^2 + |A_{2Z'}|^2}} S_{4j} - \frac{A_{1Y'} \tilde{m}_{Y'j}^* + A_{1Z'} \tilde{m}_{Z'j}^*}{\sqrt{|A_{2Y'}|^2 + |A_{2Z'}|^2}} S_{5j} \right]
 \end{aligned}$$

➔ $SX' = S_{41} k_{41}^{sx'} + S_{42} k_{42}^{sx'} + S_{43} k_{43}^{sx'} + S_{51} k_{51}^{sx'} + S_{52} k_{52}^{sx'} + S_{53} k_{53}^{sx'}$

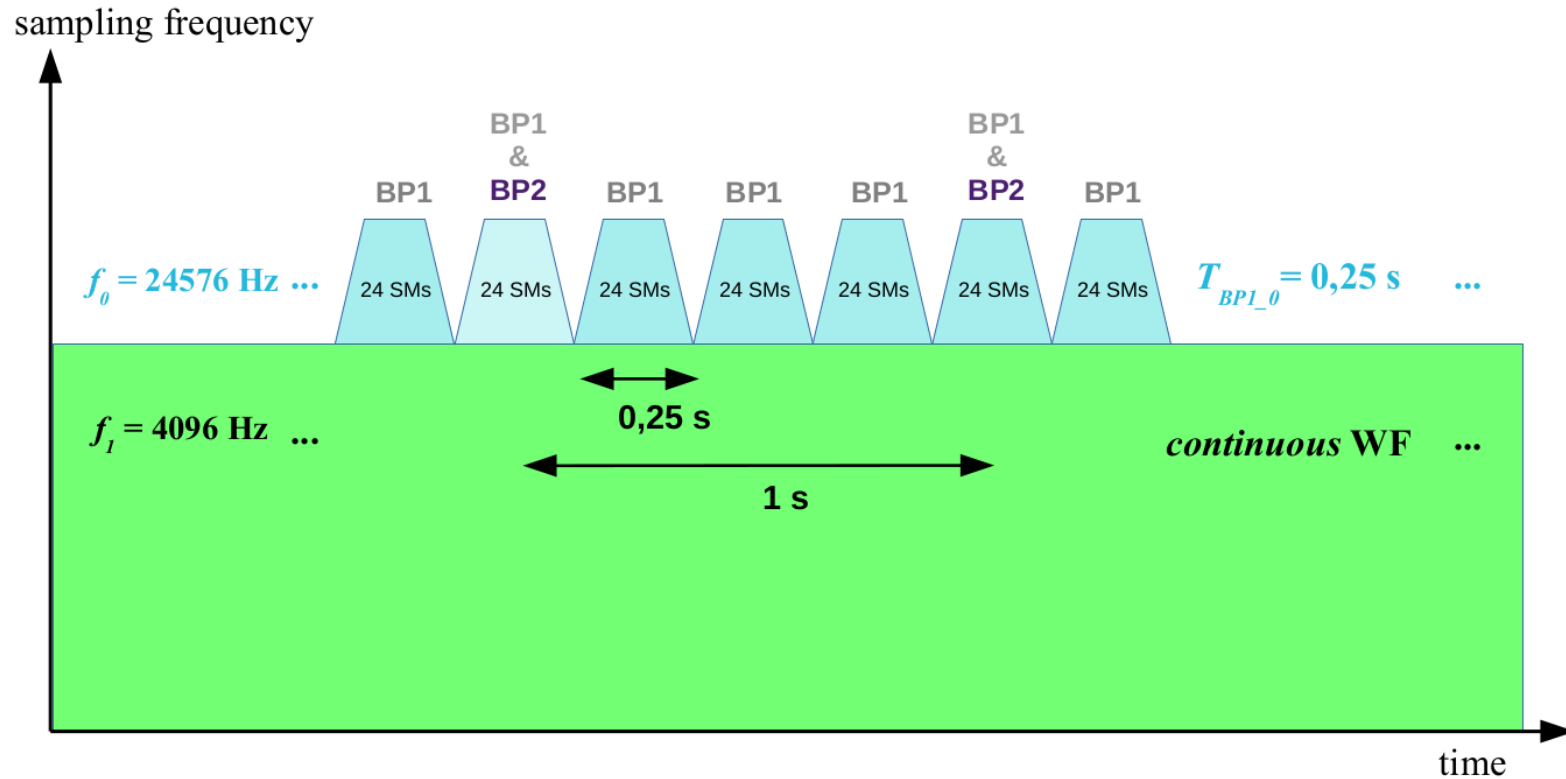
with

$$\begin{cases}
 k_{4j}^{sx'} = + \frac{A_{2Y'} \tilde{m}_{Y'j}^* + A_{2Z'} \tilde{m}_{Z'j}^*}{\sqrt{|A_{2Y'}|^2 + |A_{2Z'}|^2}} \times \exp \left[i (\varphi_{C_{1Y}} - \varphi_{A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}}) \right] & j = 1, 2, 3 \\
 k_{5j}^{sx'} = - \frac{A_{1Y'} \tilde{m}_{Y'j}^* + A_{1Z'} \tilde{m}_{Z'j}^*}{\sqrt{|A_{2Y'}|^2 + |A_{2Z'}|^2}} \times \exp \left[i (\varphi_{C_{1Y}} - \varphi_{A_{1Y'} A_{2Z'} - A_{1Z'} A_{2Y'}}) \right]
 \end{cases}$$

WARNING: As for ANT, the TF of LFR is implicitly embodied in the TF matrix of SCM (just a common calibration factor)



LFR Selected Burst Mode 1





- **Whistler waves**

Observations of whistler mode waves by the Solar Orbiter RPW Low Frequency Receiver (LFR): in-flight performance and first results, Chust, T., M. Kretzschmar, D. B. Graham et al., A & A, 2021.

Whistler waves observed by Solar Orbiter / RPW between 0.5 AU and 1 AU, Kretzschmar, M., T. Chust, V. Krasnoselskikh et al., A & A, 2021.

Whistler instability driven by the suprathermal electron deficit in the solar wind, High-cadence Solar Orbiter observations, Berčič, L., D. Verscharen, C. J. Owen, , A & A, 2021.

- **DC electric field and S/C potential measurements**

Solar wind current sheets and deHoffmann-Teller analysis: First results of DC electric field measurements by Solar Orbiter, Steinvall, K., Yu. V. Khotyaintsev, G. Cozzani et al, A & A, 2021.

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